

AZIMUTH ENVIRONMENTAL CONSULTING, INC.



Environmental Assessments & Approvals

June 18, 2020

AEC 17-069

1820839 Ontario Ltd. 950 Shoreview Drive Innisfil, Ontario L9S 5A7

Attention: Wayne Ezekiel

Re: Hydrogeological Impact Assessment Innisfil Executive Estates Phase 2 Block 39 and 41, R.P. 51M-1045, Town of Innisfil, County of Simcoe

Dear Mr. Ezekiel:

Azimuth Environmental Consulting, Inc. (Azimuth) is pleased to provide our Hydrogeological Impact Assessment for a property located in the Village of Stroud, Town of Innisfil, ON (the "Site"). This work is intended to support a Draft Plan of subdivision for the Innisfil Executive Estates Phase 2 (IEE Phase 2) development.

This evaluation focuses on the existing soil and ground water regime underlying the Site and the potential for the proposed development to impact the existing conditions. Our evaluation also includes a Reasonable Use Policy (RUP) assessment update in addition to a Water Balance evaluation to support the development of 21 lots on the above noted Site. Our assessments only addresses the Phase 2 lands, as the Phase 1 lands were previously evaluated and approved. Phase I lands were developed implementing 8 lots with tertiary treatment.

Based on the results of our analysis, it is concluded that the environmental conditions upon the Site will allow up to 21 residential lots to be developed in compliance with the Lake Simcoe Regional Conservation Authority (LSRCA's) Water Budget Policies/standards as well as the Ministry of the Environment Conservation and Parks (MECP's) RUP. This is contingent on the use of tertiary treatment technology for all 21 IEE Phase 2 lots and 8 IEE Phase 1 lots.



If you have any questions or require further information, please do not hesitate to call the undersigned.

Yours truly,

AZIMUTH ENVIRONMENTAL CONSULTING, INC.

Jackie Coughlin, B.A.Sc., P.Eng. Senior Environmental Engineer

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Jennifer Millington, M.A.Sc., P.Geo. Hydrogeologist



1.0 INTRODUCTION

Azimuth Environmental Consulting (Azimuth) was retained by1820839 Ontario Ltd. to complete a Hydrogeological Impact Assessment to support a Draft Plan of Subdivision for 21 lots for the Innisfil Executive Estate Phase 2 (IEE Phase 2) development. This study only addresses the Phase 2 lands, as the Phase 1 lands were previously evaluated and approved.

The purpose of this assessment is to characterize the existing hydrogeological conditions at the Site and the potential for the proposed IEE Phase 2 development to impact the existing environmental conditions including the potential for adverse effects from the proposed new sewage systems on local ground water resources.

A portion of the Site is considered a Significant Ground Water Recharge Area (SGRA) and the entire Site is considered a Highly Vulnerable Aquifer (HVA). The Site is also located within a Wellhead Protection Area D (WHPA-D) but is not in a WHPA-Q1 or WHPA-Q2. The Site is within 500m of a municipal well and is within the 25-year Capture Zone Boundary. Due to the Site's classification as a Major Development and its location within a SGRA, it is subject to the LSRCA's Water Budget policy and therefore a water balance was completed for the Site.Given that the proposed development is located within the WHPA-D boundary of a municipal well field, conformity with Source Water Protection and the Clean Water Act has also been evaluated as part of this work.

The remainder of this report presents the background information and provides the results of our evaluation and associated conclusions and recommendations.

2.0 BACKGROUND

The Site is located on the east boundary of the community of Stroud. The legal description of the Site is Block 39 and 41, Plan 51M-1045 (Part of Lot 17, Concession 10, in the former Geographic Township of Innisfil, Town of Innisfil, County of Simcoe, Ontario) (Figure 1).

The first phase of the IEE development ("IEE Phase 1")was approved in 2015 by the Town of Innisfil and included 38 single detached residential lots, internal roadways, a stormwater management block (Block 42) and two vacant blocks (Block 41 and 39) designated for future development (Figure 2).

The second phase of the IEE development ("IEE Phase 2") consists of future development Blocks 39 and 41 (4.78 hectares / 11.81 acres) which will be subdivided for the creation of 21 single detached residential lots (Figure 3). The Phase 2 draft plan also



includes an internal roadway from Robinson Avenue (0.569 hectares/1.406 acres), appropriate buffers from the Metrolinx railway line (0.385ha/0.951aces), and the berm area to be transferred to the Town of Innisfil (0.222 ha. / 0.547 ac). Each lot will incorporate tertiary treatment with inground disposal of the treated effluent. Water supply will be provided from the Town of Innisfil.

As part of IEE Phase 1 development, Azimuth completed a Reasonable Use Policy (RUP) assessment for the IEE Phase 1 development. The RUP assessment was accepted and resulted in the approval of 38 residential lots on conventional treatment systems (Azimuth, 2011). The RUP assessment has since been updated to reflect the IEE Phase 2 development for 21 lots. The ability to meet the MECP's RUP for the proposed development is contingent on the use of tertiary treatment technology for Phase 2 and the use of tertiary treatment units (TTU's) on 8 lots in the previously approved IEE Phase 1 development. TTU's have now been installed on Lots 8 in the IEE Phase 1 subdivision (Appendix D). The updated RUP assessment is provided in Section 6.0 of this report.

2.1 Adjacent Land use

Adjacent land use consists of existing single detached residential development to the south and west within the Village of Stroud (and includes the IEE Phase 1 residential subdivision), agricultural farm land to the north, the Metrolinx Railway to the east, and agricultural farm land and some rural residential dwellings to the east situated outside the settlement area boundary of Stroud).. There is one single detached residential dwelling (Robertson residence) located adjacent the southwest corner of the IEE Phase 2 development.

2.2 Information Sources

Our assessment considered available literature data / technical reports for the Site as well as the completion of an on-Site field program (*i.e.*, soil, ground water monitoring). Information provided by the following sources was utilized in the course of this evaluation:

- Reasonable Use Assessment IEE Phase 1 (Azimuth, 2011);
- Geotechnical Investigation (Terraprobe, 2011);
- Functional Servicing and Storm Water Management Report (WMI Engineering, (2020);



3.0 ENVIRONMENTAL SETTING

3.1 Physiography and Soils

Physiographically, Chapman and Putnam (1984) define the Site as part of a region known as the Peterborough Drumlin Fields. Most of this region is located to the south and east of Lake Simcoe, although the Site is within the western edge of a smaller portion of the drumlin field located just south of Kempenfelt Bay.

The Soil Map of Simcoe County (Canada Department of Agriculture, 1959) defines the surficial soils as part of "Bondhead Sandy Loam" that is grey, calcareous and exhibits good drainage characteristics. The Quaternary Geology Map of Ontario (Barnett, *et al.*, 1991) states that the main surficial soil unit is classified as "Newmarket Till", which generally consists of a sandy silt to silt matrix containing moderate to high levels of carbonate and clasts.

Although the majority of Stroud is serviced by a municipal drinking water system, a review of the local MECP well records and the 2004 Golder South Simcoe Ground Water (SSGW) Study for the Town of Innisfil (Stroud) was undertaken to compile supporting hydrogeological data for the Site. The stratigraphic descriptions provided in water well records acquired from the MECP records indicate a surficial layer of sand, silty sand and/ or sand clay mixtures (<10m), underlain by a fine to medium sand layer (10-25m thick). Below the fine to medium sand are moderately thick, alternating clayey/ sandy silt and fine grain sand/ sand gravel mixtures which extend to >60 metres below ground surface (Golder *et al.*, 2004).

3.2 Topography and Site Drainage

The local topography of the area is defined as smooth to gently sloping. The Site has no marked relief, with a majority of the development sloping to the southeast towards the stormwater management pond situated adjacent along the south boundary of the IEE Phase 2 development. Elevations range from ~275metres above sea level (m asl) to ~268 m asl across the Site.

Shallow ground water on the Site would be controlled by the topography and thus would flow in a southeasterly direction towards the storm water management pond. Regional ground water flow is towards Lake Simcoe.

3.3 Hydrogeology

3.3.1 Municipal Supply

The SSGW Study for the Town of Innisfil (Golder *et al.*, 2004) indicates the presence of two shallow aquifers (A1 and A2) and two (2) deep aquifers (A3 and A4) within the



general area of Innisfil. The majority of the municipal water supply systems in Innisfil utilize the deeper aquifer units, which are typically found at elevations below 200m asl.

Flow in the upper aquifer system is primarily influenced by the local topography and drainage and flow in the lower aquifer systems are influence by the bedrock topography and the regional hydrogeological features.

The Golder *et al.*, (2004) report provides greater detail of the Site because of it location relative to the Stroud municipal wells. As shown in Figure 9.2.2 of the South Simcoe Ground Water (SSGW) Study, the shallow aquifer system (A1/A2) is present at elevations above 200 m asl within the vicinity of the study area and the deeper aquifer system is present at ~155-195 m asl (A3). The shallow aquifer system is composed of fine grained sand and/or sand and gravel and is separated by a ~20-30m thick confining layer consisting of clayey silt, clay and sandy silt and clay. Aquifer A3 is separated from A2 by a 20-30m thick silt and clayey confining layer.

The Stroud municipal drinking water system obtains its water from two (2) municipal wells (Wells 2 and 3) both of which pump from regional Aquifer A3 which is reportedly overlain by 60m or more of till material with intervening aquifers as described above (Golder *et al.*, 2004).

3.3.2 Private Wells

At this property and in the general area of Stroud, the shallow aquifer is not the preferred potable water source because of potential connections to surface contaminant sources from septic beds located upgradient of the Site. As such, the deeper aquifer system is primarily used to supply water in the Village of Stroud.

The closest private well to the Phase 2 development is located on the Robertson property, adjacent the southwest corner of the IEE Phase 2 development. According to the well record, the well is 23.2m deep and consists of 3m of layer of sand overlying 7m of clay overlying 12.5 m sand (see Figure 6).

A well survey of the area downgradient of the Site was completed by Azimuth however mapping provided by InnServices indicates that servicing is provided along Victoria Street (west of the tracks), thus many of the dwellings to the south of the Site are presumed to be connected to the municipal drinking water system. Most of the wells (existing or otherwise decommissioned) are between 20-50 years old and target or previously targeted the shallow or intermediate aquifer at an average depth of 18m bgs.



There are a few dwellings situated east of the railway line. Mapping indicates that the closest well to the Site would be located~60m to the east of the Site however no information could be obtained about the location and/ or type of well from the owner and/ or MECP well record database. The next closest well is a drilled well located ~150m to the east-southeast however no information could be obtained from the MECP well record database. In general, most of the drilled wells in this area are old (1960's) and appear to have been previously dug wells according to the well records. Well depths range between 12.8m and 33.5m bgs.

4.0 HYDROGEOLOGY EVALUATION

4.1 Soil Investigations

Previous soils investigations which included the IEE Phase 1 development were completed by Geospec Engineering Ltd. (Geospec) in 2010. As part of these field investigations a total of eight (8) boreholes (BH-1 thru BH-9) were excavated to between 3.3 and 5.2 m bgs. Three boreholes were retrofitted as wells (i.e., G-3, G-8 and G-9).

Five of the excavations (BH-1 thru BH-8) were completed within the IEE Phase 1 development lands; and two excavations (BH-7 and BH -9) were completed within the IEE Phase 2 development lands including testwellG-9. Test well G-9 (now abandoned) is located within the centre part of IEE Phase 2 and is ~5.2m deep. BH-7 was located in the southwest corner of the Phase 2 area and is 5m deep (Figure 4).

The surficial soil descriptions provided by Geospec indicate a silt & sand/ sand & silt till in the IEE Phase 1 area and a silt till with some sand and gravel underlain by sand and silt deposits in the southeast part of the Site. Perched ground water conditions were noted in the southeast part of the Site (Geospec, 2011).

In support of the Phase 2 development plan, supplementary test pitting and soil sampling was completed by Azimuth in October 2017 and in March 2018. The purpose of the soil sampling was to identify the native soils, as well as the presence or absence of a shallow ground water table within the IEE Phase 2 lands.

A total of thirteen test pits (TP-1 through TP-13) were excavated to \sim 3m bgs, seven (7) of which were retrofitted with a standpipe for the purposes of monitoring shallow water table conditions. Test pits 1through 5were excavated within the north to the central part of Site and TP- 6 through TP-13 were excavated within the south part of the Site. Water levels were monitored at seven locations and at Geospec's Test well G-9.



The overburden soils in the north part of the Site can be described as silty sand and gravel. The overburden soils in the south part of the Site can be described as sand with a trace of silt. Ground water was not observed in any of Azimuth's test pits.

4.1.1 Grain Size Analysis

At the conclusion of Azimuth's field investigation, nine representative surficial soil samples were submitted to Terraprobe for grain size analysis and permeability testing ('T' time). The purpose of this testing is to characterize the grain size distribution for the shallow overburden soils, as well as to determine an estimated infiltration rate ('T' time)/ permeability rate for use in the design of the future septic beds.

The location of the test pits is provided on Figure 4 and the grain size reports are provided in Appendix B. The permeability of the native materials varies somewhat across the Site from a lower permeability soil being observed in the north half to a much higher permeable soil observed in the south half. Percolation rates ranged between 45-50min/cm at two locations within the north part and between 2-12min/cm at the seven remaining locations.

Location	Depth	Unified Soil	Soil Description	T-Time
	m bgs	Classification		(min/cm)
	(feet)			
TP-1	0.6(2)	SM	Silty Sand, some Clay, trace gravel	45-50
TP-3	0.6(2)	SM	Silty Sand, trace gravel, trace silt	2-4
TP-4	0.9(1)	SW-SP	Gravelly sand, trace silt	4-6
TP-6	0.6(2)	SM	Silty Sand, some Clay, trace gravel	45-50
TP-7	1.8 (6)	SP	Sand with trace silt, trace gravel	3-5
TP-8	1.8 (6)	SW-SP	Sand and Gravel with trace silt	2-4
TP-10	1.8 (6)	SP	Sand with trace silt, trace gravel	4-6
TP-11	1.0 (3)	SW-SP	Sand with some silt, some gravel	10-12
TP-12	1.2 (4)	SP	Sand with trace silt, trace gravel	4-6

Table 1: Soil Summary

4.1.2 Ground Water Monitoring

Ground water monitoring was completed at seven monitoring locations (TW-1 through TW-7) as well as at Terraprobe's existing monitoring well location (G9) between October 6, 2017 to August 29 2018. This includes manual measurements taken in March, April, and June 2018 to capture high water table conditions during spring freshet. With the exception of TW-3, TW-6, TW-7 and G9, all monitoring locations were dry (Figure 5).

In that regard, the water level was measured at depths between 1.7 and 4.3m bgs. The highest water levels were observed in March 2018at TW-3, TW-6, and TW-7 and April 2018at G9 (Table 2). It is noted that upon installation, the end cap of TW-6 and TW-7



was not punctured to allow for the drainage of collected water. This technique was applied for the remaining well locations. Since these two locations were the only wells to have recorded water levels in March, and since the recorded water level was less than 10cm above the base of the well (i.e. within the well cap and not within the screen as water within the screen has migrated back into the overburden), these measurements are not considered representative of the water table elevation. The high water level condition is therefore considered to be the levels measured in April, which are shown in red text and bold in Table 2.

Monitoring	Location	Well	Ground	March 7,	April 26,	June 12,
Location	Relative to Site	Depth	Elevation	2018	2018	2018
	Boundary	(mbgs)	(masl)	mbgs/masl	mbgs/masl	mbgs/masl
TW-1	North	2.75	272.0	dry / <269.3	dry / <269.3	dry / <269.3
TW-2	Central	2.83	272.5	dry / <269.7	dry / <269.7	dry / <269.7
	northwest					
TW-3	Central west	2.61	272.0	dry / <269.4	1.91 / 270.1	dry / <269.4
TW-4	Southwest	2.60	269.0	dry / <266.4	dry / <266.4	dry / <266.4
TW-5	Central east	2.20	270.0	dry / <267.8	dry / <267.8	dry / <267.8
TW-6	Central east	2.95	268.0	2.93 / 265.1	dry / <265.1	dry / <265.1
TW-7	Southeast	3.10	267.5	3.03 / 264.5	dry / <264.4	dry / <264.4
G9**	Center of Site	5.13	271.4	3.61 / 267.8	1.70 / 269.7	4.33 / 267.1

Table 2:	Ground	Water	Level	Measurements
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** Terraprobe well, 2011

Water level measurements are expected to fluctuate seasonally, particularly during periods of high precipitation and spring runoff. The presence of high water at TW-3 and G9 may indicate the presence of a localized perched condition. Based on the above, ground water control measuring during excavations may be required during foundation construction if work is completed in the spring. It is therefore recommended that construction occur in the dry summer months to reduce or eliminate the need for temporary dewatering.

5.0 WATER BALANCE

In order to determine the potential changes to the natural ground water recharge conditions, a pre- and post-development water balance assessment has been completed using the Thornthwaite and Mather method (1957). This method evaluates evapotranspiration based on precipitation and temperature. Residual soil saturation is a function of topography and soil type. Monthly data are tabulated from daily average temperature and precipitation, and the water budget is a continuous calculation over the period of record. To clarify, the method and the approach used by many individuals in examining infiltration resets annual conditions (moisture deficit, snow storage, etc.) over the winter months because of the general lack of infiltration during the frost period.



However, we maintain those records and carry them forward from month to month during the entire period of record.

Values were determined on a monthly basis, compiled from daily Environment Canada meteorological data station located in Barrie, Ontario between 1970 and 2017 (Station ID 6110557). The calculations are based on the average conditions during this period; the average precipitation was 908 mm, rainfall was 655 mm, evapotranspiration was 484 mm and the surplus was 424 mm.

5.1 Land Use

5.1.1 Pre-Development

The entire pre-development Site area can be classified as meadow land use (Table 3).

Table 3:	Pre	Develo	oment	Area	Classification
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Land Use		Land Area (m ²)
Meadow		47,800
T	OTAL	47,800

Land within the pre-development scenario is considered 0% impervious.

5.1.2 Post-Development

Land within the post-development Site is considered landscaped grass, driveway, roads, sidewalk, and structures. The post-development land area is summarized in the below Table 4:

Land Use	Land Area (m ²)					
Landscaped Grass	39,322					
Driveways	1,320					
Roads	2,438					
Sidewalk	540					
Structures	4,180					
TOTAL	47,800					

 Table 4: Post-Development Area Classification

Land within the post-development scenario is considered 18% impervious. The impervious area is associated with the structures, driveways, sidewalks, and internal roads.



5.2 Infiltration

Infiltration factors for the Site were estimated based on the underlying soil, local topography, and ground cover as per Table 2 of the Ministry of Environment and Energy (MOEE) Hydrogeological Technical Information Requirements for Land Development Applications (1995).

The soil variable factor was determined by taking into account information obtained from the previous field programs completed for the Site (Section 4.1.1). This information confirms that the surficial material is composed primarily by a silt/sand material.

The infiltration factors utilized in the water balance assessment are summarized in Table 5 below.

Land Use	Infiltration Factor	Assumption
Meadow	0.65	Rolling land, sand/silt soil, meadow land
Landscaped	0.60	Rolling land, sand/silt soil, lawn

Table 5: Summary of Pervious Land Infiltration Factor

5.2.1 Pre-Development

Pre-development infiltration was determined by multiplying the annual average surplus amount, the area of each land use, and the infiltration factor for each land use. The pre-development annual infiltration is therefore 13,174 m³/year from meadow land (Appendix C).

5.2.2 Post-Development

Post-development infiltration (without mitigation) was determined by multiplying the annual average surplus amount, the area of each land use, and the infiltration factor for each land use. The post-development annual direct infiltration is therefore 10,004 m³/year from landscaped grass. There is therefore a decrease in infiltration of 3,170 m³/year from pre- to post-development without mitigation which represents 24%.

As noted above, the Site is considered a HVA and SGRA within a WHPA-D. Sites located within a HVA may have restrictions on the type or location of LIDs employed for additional infiltration. However, since the Site is considered low density residential, it is our understanding that there are no applicable infiltration restrictions.

Additional infiltration will be gained by directing rooftop runoff toward the adjacent grass surface. There is approximately $4,180 \text{ m}^2$ of rooftop area which will contribute to indirect infiltration. The infiltration volume for rooftop downspouts is determined by multiplying the area $(4,180 \text{ m}^2)$ by the annual rainfall (655 mm) by the infiltration



coefficient of the receiving land use (0.60) and by 80% to account for a 20% evapotranspiration factor. The total infiltration gained through this method is 1,314 m³/year. This brings the total infiltration to 11,318 m³/year in the post-development (with mitigation) scenario which leaves a deficit of 1,856 m³/year.

Through consultation with WMI & Associates Limited it is our understanding that a grass swale network will be used around the perimeter of the proposed development to capture runoff and convey this water to the storm water management pond. It is assumed that the majority of overland flow within the Site will be conveyed toward this feature.

Grain size analysis was completed at numerous locations across the Site (Section 4.1.1). Percolation rates ranged between 45-50min/cm at two locations within the north part and between 2-12min/cm at the seven remaining locations. Due to the variability in material, a conservative value of 45 min/cm (or 320 mm/day) was utilized for swale infiltration.

The water balance currently has a deficit of $1,856 \text{ m}^3$ /year. If it is assumed that infiltration within the swale network will occur over 15 days, then the grass swale will be required to cover an area of 772 m². This was determined by dividing the required volume ($1,856 \text{ m}^3$) by the length of infiltration (15 days), and by the infiltration rate (320 mm/day). The swale area was then multiplied by a conservative factor of 2. This represents a swale 1m by 772m long or 2m by 386m long swale network. This methodology assumes that the swale will be positioned so that it can collect the majority of runoff from the Site and that the runoff is available for infiltration. It is our understanding that this will be considered/ incorporated by WMI & Associates Limited into the storm water design.

Based on the information summarized in Section 4.1.2 the high water level at the Site is at maximum 1.7 mbgs. Significant grading is not anticipated prior to development. Since the incorporated LIDs will occur at the ground surface there is at least a 1m vertical separation between the high ground water table and the proposed LIDs (rooftop diversion and conveyance swale).

5.2.3 Water Balance Summary

Using the climate model data and calculations mentioned above, the following pre and post-development infiltration values have been summarized (Appendix C).

Ground water infiltration at the Site could decrease by up to approximately 24% if no mitigation measures are employed. This reduction is based on the creation of impervious surfaces associated with driveways, sidewalks, roads, and structures. The 24% reduction equates to approximately $3,170 \text{ m}^3/\text{year}$.



The reduction is eliminated when mitigative strategies are employed (i.e. rooftop diversion and swale conveyance network. The LIDs account for an additional 3,170 m³ of infiltration per year, which brings the total post-development infiltration volume to match the pre-development infiltration volume. As such, the water balance for the Site meets the Lake Simcoe Region Conservation Authority (LSRCA) requirements.

5.3 Well Head Protection Areas

As indicated in Section 4.2 of the Town of Innisfil's Official Plan, well head protection areas were defined in the South Simcoe Ground Water Study (2004). The study identifies areas around municipal wells susceptible to ground water contamination.

As presented in Figure 9.6.1 of the South Simcoe Ground Water Study, the proposed development is located within the "25-year capture zone boundary" of the Stroud municipal well field. Although the Site is located in close proximity to these wells, the capture zone extends to the southeast, which would indicate that the subject development property is downgradient of the municipal well locations.

Furthermore, the Stroud water supply system obtains its water from regional Aquifer A3 which is less than 200 m asl and is overlain by ~60 m of till material (Golder *et al*, 2004). The SSGW study also indicates that the capture zones for the Stroud well field are completely within a medium vulnerability area (Golder *et al.*, 2004); however, the vulnerability is more representative of the shallow unconfined aquifer and does not reflect the 60 m thick aquitard that exists between the shallow aquifer and the municipal aquifer.

6.0 GROUND WATER / RUP ASSESSMENT

As part of the IEE Phase 1 development, Azimuth completed a Reasonable Use Policy ("RUP") assessment for the entire parcel of land. The RUP assessment was accepted and resulted in the approval of 38 residential lots, each serviced by a conventional treatment system (Azimuth, 2011). The RUP assessment is now being updated as part of this Report to reflect the IEE Phase 2 development containing 21 lots. The ability to meet RUP is contingent on the use of tertiary treatment units (TTUs) for all 21 lots and the installation of TTUs on 8 lots located within the previously approved IEE Phase 1 subdivision. TTU permits for the applicable Phase 1 lots are provided in Appendix D.

Tertiary treatment technology can reduce nitrate concentrations to between 15 - 25mg/L (NO₃-N) with an average 20mg/L depending on the technology used. In this case, a Norweco's Hydro-Kinetic FEU system is considered a typical system that could be used, reporting a removal rate of 67% for total nitrogen. For the purposes of demonstrating



compliance with the RUP, the calculations include 21 Phase 2 TTUs, 8 Phase 1 TTUs and 30 Phase 1 conventional septic systems.

6.1 Private Well Evaluation

The primary focus of the ground water assessment is on impacts to off -site downgradient wells from septic beds. The closest private well to the IEE Phase 2 development is located on the Robertson property, located near the southwest corner of the Phase 2 development. The drilled well is located within the northwest corner of the Robertson property (Figure 6). The target aquifer is overlain with 7 m of clay which should be sufficient to protect this well from surface water contaminants, however sampling would be required to confirm this assumption.

According to the MECP well database, there are a number of wells located along Victoria Street to the south and southeast of the Site. Most of these wells (existing or otherwise decommissioned) are between 20-50 years old and target or previously targeted the shallow or intermediate aquifer at an average depth of 18m bgs. Although mapping from InnServices illustrates some of the dwellings along Victoria Street are municipally serviced, there are 2 dwellings located immediately adjacent Lots 20 and 21 of the IEE Phase 2 development that may not be municipally serviced (See Figure 6). No wells could be observed at the front or rear of these properties however the aerial imaging suggests that septic beds are located within the rear of these lots thus any wells (if present) would be located along the front or side of the dwelling to adhere to the minimum Ontario Building Code (OBC) setbacks between wells and septic systems (i.e., 15m-30m). If wells do exist on these properties, the proposed septic beds on Lots 20 and 21 can be strategically placed to maximize OBC setbacks between the proposed bed locations and any off site wells.

For the remainder of the Site, the treated effluent discharging to the proposed disposal beds would flow with shallow ground water in a southeasterly direction. Most of the wells along Victoria Street (if present) would also be located at the front of these properties (>100m away from the Phase 2 property), to maximize wells setbacks from their own septic systems located within the rear of these properties. Any wells situated on the east side of the railway line are more transgradient to the flow of ground water from the Phase 2 Site therefore impacts would not be anticipated.

6.2 Reasonable Use Policy Assessment

A ground water assessment is typically evaluated within the scope of the MECP Reasonable Use Policy (RUP Procedure B-7-1), the 2008 MECP Guideline for Sewage Works (MECP, 2008) and/ or MECP Procedure D-5-4 (MECP, 1996). The RUP



describes acceptable levels of parameters that are permitted to reach the downgradient property boundary in the ground water regime.

In general, RUP is only applicable to large sewage works with a point source discharge (i.e., treatment systems that generate >10,000 Lpd). As the sewage volumes for each lot are significantly less than 10,000 Lpd, they are regulated under the OBC. Therefore, RUP does not strictly apply in this case however can be used as a guide to determine concentration levels at the downgradient property boundary and evaluate any undesirable environmental impacts from sewage disposal systems.

6.2.1 RUP Assumptions

The following assumptions were used in the RUP evaluation:

Nitrate Criteria: Nitrate (as nitrogen) is the main contaminant of concern for sewage works that discharge effluent to the ground water regime due to the potential for health related impacts in drinking water supplies. Under a Reasonable Use evaluation, the quality of drinking water must not be degraded by an amount in excess of 25% of the difference between background concentrations and the ODWQS for health related parameters (i.e., 10 mg/L for nitrate-N). Historical use of RUP has accepted the maximum compliance criteria for nitrate at the downgradient property boundary as 10 mg/L (ODWQS for nitrate-N) for residential lot development. For the purposes of this assessment, a value of 10 mg/L (nitrate-N) was used as the maximum RUP compliance criteria.

Dilution Area: RUP considers dilution only, and therefore it is highly conservative. Because an individual lot is relatively small, and infiltration from the full lot contributes to dilution, thus the entire property (4.78ha) is used for the dilution calculation. This includes areas designated for internal roads, the Metrolinx widening and other lands transferred to the Town.

Background Nitrate: MECP Guideline B-7-1 describes the background concentration to be used in the RUP calculations as "Background is considered to be the quality of ground water prior to any man-made contamination." Any elevated nitrate concentrations observed at the Site are assumed would be related to agricultural fertilizer application, and therefore a pre-anthropogenic background of 0.2 mg/L is appropriate for this variable and is consistent with the MECP guideline since RUP uses this variable to reflect the concentration of the precipitation infiltrating on the property.

The value of ~ 10 mg/L reflects the shallow ground water condition and represents the water that is underflowing the Site from upgradient areas, which is not used in the RUP



calculation. However, the RUP allows the reviewer to consider site conditions in evaluating the "reasonable use" of the receiving ground water regime. In this case, the shallow ground water regime has been impacted by nitrate levels from both agricultural practices and septic inputs from the existing Stroud community. As described in Guideline B-7 (Section 4.1), it is appropriate for the proposed development to discharge septic effluent into the shallow unit, reflecting its "reasonable use", as it has been contaminated and the contamination is expected to continue.

Influent Nitrate Concentrations: Typical nitrate (NO₃-N) values for weak to medium domestic sewage for a standard Class IV system range between 20 and 60mg/L (Metcalf & Eddy, 1972.) with an average concentration of 40 mg/L (NO₃-N). However, tertiary treatment can reduce nitrate concentrations by 50-67% (e.g., WBS, Norweco's Hydro-Kinetic FEU system) depending on the technology used. Using the above tertiary treatment technologies, nitrate concentrations can be reduced to between 15 – 25mg/L (NO₃-N) with an average 20mg/L. For the purposes of this assessment, a nitrate concentration of 20mg/L is used for tertiary treatment and 40mg/L is used for conventional treatment.

Annual Sewage Volume: The average daily volume for a single residential home is typically between 800-1000Lpd. As per Procedure D-5-4 (MECP, 1996), the volume of sewage should not exceed 1,000Lpd when evaluating contaminant attenuation for residential development. For the purposes of this assessment, 1000Lpd is used.

Infiltration Rates: In 2008, the MECP modified the RUP assessment and have incorporated a constant quantity of dilution in the calculation (MECP, 2008). The quantity is 250mm of water per year (mm/a) over the area of the contaminant plume. For the purposes of the RUP evaluation, an average infiltration rate of 279.5 mm/a is used since it represents Site specific conditions (see below) The infiltration rate is lower than that used in the original 2011 RUP evaluation reflecting an updated water budget analysis.

As part of this evaluation, a water budget was prepared using the Thornthwaite and Mather (1957) method using the Environment Canada meteorological data at Station 6110557 (Barrie) between 1970 and 2018. The average annual water surplus is 430 mm representing the amount of water available annually to infiltrate into the ground water or run off as surface water. During this period, the average annual precipitation was 912 mm, the average annual rainfall was 657 mm, and the average annual evapotranspiration was 481 mm. Snowmelt accounts for 255 mm of the annual surplus and the remainder (175mm) is split between runoff and infiltration in the non-freezing times of the year (rain surplus). Considering that the surficial geology within the study,



the majority of the site being cultivated and the flat nature of the topography, it was determined that between55 to 75% (average 65%) of the water surplus will infiltrate across the Site. By multiplying the annual average precipitation surplus amount (430) by the soil infiltration rate (65%), infiltration is estimated to be approximately 279.5 mm/year for the Site.

6.3 Prediction of Contaminant Attenuation

The nitrate concentration at the Phase 2 development boundary can be estimated using the nitrate dilution equation:

$$C_{pb} = \frac{Q_1 C_1 + Q_2 C_2}{C_T}$$
 where,

- Q₁ = dilutions area (m²) x infiltration (m/a) = total development area (m²) x infiltration rate (m/a);
- $C_1 = (background nitrate concentration from precipitation) \sim 0.2 mg/L;$
- $Q_2 = (annual sewage volume) = 1,000 Lpd (MECP, 1996);$
- C₂ = (effluent NO₃-N concentration in sewage) = 40.0 mg/L (conventional treatment) or 20mg/L (tertiary treatment);
- $Q_T = (\text{total offsite sewage volume}) = Q_1 + Q_{2};$
- C_{pb} = contribution of nitrate at downgradient property boundary is $\leq 10 \text{ mg/L}$.

IEE Phase 2 Development:

- Q_1 = Phase 2 dilution area (m²) x infiltration (m/a) = 47,800 m² *179.5 m/a infiltration = 13,360 m³/a);
- $C_1 = (background nitrate concentration from precipitation) = ~ 0.2 mg/L;$
- $Q_2 = (Phase 2 sewage volume) = 1,000x 21 = 21,000 Lpd;$
- $C_2 = (effluent NO_3-N concentration in sewage) = 20mg/L (tertiary treatment);$
- $Q_T = (\text{total offsite sewage volume}) = Q_1 + Q_{2;}$
- C_{pb} = contribution of nitrate at downgradient Phase 2 boundary is ≤ 10 mg/L.

Based on the above assumptions, the average nitrate-N concentration at the Phase 2 Site boundary is estimated to be 7.4 mg/L. The RUP results indicate that the average loading at the Site boundary is below the 10 mg/L criteria, thus the MECP RUP is met for the IEE Phase 2 development. A sensitivity analysis was also completed using a higher



effluent NO₃-N concentration (25 mg/L NO₃-N) and the results indicated an RUP value is ≤ 10 mg/L; therefore our approach is considered conservative.

IEE Phase 1 and Phase 2 Development:

As part of the technical evaluation undertaken in support of the IEE Phase I development, Azimuth completed a Reasonable Use Policy evaluation for the 17.5 ha parcel of land (Azimuth, 2011). The RUP assessment was accepted and resulted in the approval of 38 residential lots with conventional sewage treatment systems. In order to comply with MECPs RUP at the property boundary as a result of the Phase 2 development, the owner has installed eight (8) of the 38 previously approved conventional systems with tertiary treatment. In that regard, the RUP calculation was re-evaluated having consideration of cumulative impacts from both phases based on the following:

- 38 IEE Phase 1 development lots:
 - ➢ 30 conventional systems, and
 - ➢ 8 tertiary treatment systems.
- 21 IEE Phase 2 development lots (4.78ha):
 - 21 tertiary treatment systems

The nitrate concentration at the property boundary was estimated using the following equation:

$$C_{pb} = \frac{Q_1C_1 + Q_2C_2 + Q_3C_3 + Q_4C_4}{C_T}$$
 where

- Q_1 = dilutions area (m²) x infiltration (m/a) = 175,520 m² *179.5 m/a infiltration = 48,959 m³/a;
- $C_1 = (background nitrate concentration from precipitation) = ~0.2 mg/L;$
- $Q_2 = (Phases I sewage volume) = 1,000 x 30 units total = 30,000 Lpd;$
- C₂ = (effluent NO₃-N concentration in sewage) = 40.0 mg/L (conventional treatment
- $Q_3 = (Phase I sewage volume) = 1,000 x 8 units total = 8,000 Lpd;$
- C_3 = (effluent NO₃-N concentration in sewage) =20 mg/L (tertiary treatment)
- $Q_4 = (Phase 2 sewage volume) = 1,000 x 21 units total = 21,000 Lpd;$
- C_4 = (effluent NO₃-N concentration in sewage) =20 mg/L (tertiary treatment)



- $Q_T = (\text{total offsite sewage volume}) = Q_1 + Q_2 + Q_3 + Q_{4;}$
- C_{pb} = contribution of nitrate at downgradient property boundary is $\leq 10 \text{ mg/L}$.

Using the same general assumptions provided in Section 6.1.1, the average nitrate concentration at the property boundary is estimated to be 9.4mg/L. Based on the previous installation of 8 conventional systems with TTU's for the IEE Phase 1 development and by incorporating TTU's for all 21 Phase 2 lots, the net loading is below the 10 mg/L criteria. Therefore, we conclude the RUP guideline is met.

The results of the RUP assessment are considered to be conservative for individual lot development since Reasonable Use Policy is intended to be used to evaluate larger volumes of sewage from large wastewater treatment systems. As the proposed dwellings will be serviced by municipal water, there are no ground water wells proposed for the site. The deeper aquifer system will be used to supply water to the area.

7.0 CONLUSIONS AND RECOMMEDATIONS

The nitrate dilution calculation was used as a guide to determine concentration levels at the downgradient boundary to evaluate any undesirable impacts from the sewage works from the IEE Phase 2 development. In this case, the results of the assessment show that the net loading at the property boundary meets the 10 mg/L criteria provided that tertiary treatment technology is used with a greater than 50% removal rate for nitrate-N for all 21 Phase 2 lots and 8 Phase 1 lots. The use of tertiary technology is sufficient to protect the natural environment and will not result in any negative impact on the ground water quality.

Based on the physical characteristics of the Site, nitrate concentrations in the shallow subsurface would also be significantly reduced by nitrification and attenuation processes, as well as biological uptake, which are not considered within the RUP methodology. Denitrification also plays a primary role in polishing nitrate concentrations in the shallow subsurface will is also not factored in the RUP methodology. As such, impacts are expected to be minimal in nature as a result of the proposed development.

Ground water infiltration at the Site could decrease by approximately 24% if mitigation measures are employed. This reduction is based on the creation of impervious surfaces associated with driveways, sidewalks, roads, and structures. The 24% reduction equates to approximately 3,170 m³/year. The reduction is eliminated when mitigative strategies are employed (i.e. rooftop diversion and swale conveyance network. The LIDs account for an additional 3,170 m³ of infiltration per year, which brings the total post-development infiltration volume to match the pre-development infiltration volume. As



such, the water balance for the Site meets the Lake Simcoe Region Conservation Authority (LSRCA) requirements.

8.0 REFERENCES

- Barnett, P.J. Cowan, W.R. and Henry, A.P. 1991. Quaternary Geology of Ontario, southern sheet; Ontario Geological Survey, Map 2556, Scale 1:1,000,000.
- Canada Department of Agriculture, 1959. Soil Map of Simcoe County, Ontario; South Sheet. Soil Survey Report No. 29.
- Chapman, L.J. and D.F. Putnam, 1984. The Physiography of Southern Ontario. 3rd Edition, OGS Special Volume 2, MNR, ISBN 0-7743-9422-6.
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- MMAH, 1997. Ontario Building Code, Part 8 Sewage Systems. Ont. Reg. 403/97 made under the Building Code Act, 1992. As amended from time to time.
- Ministry of the Environment, 1982. Manual of Policy, Procedures and Guidelines for Onsite Sewage Systems. Queen's Printer for Ontario, ISBN 0-7743-7303-2.
- Ministry of the Environment, 1996. Procedure D-5-4 Technical Guideline for Individual On-Site Sewage Systems: Water Quality Impact Assessment.
- Ministry of the Environment. 2006 (revision). Technical Support Document for Ontario Drinking Water Standards, Objectives, and Guidelines
- Ministry of the Environment, 2008. Design Guideline for Sewage Works. PIBS6879.



APPENDICES

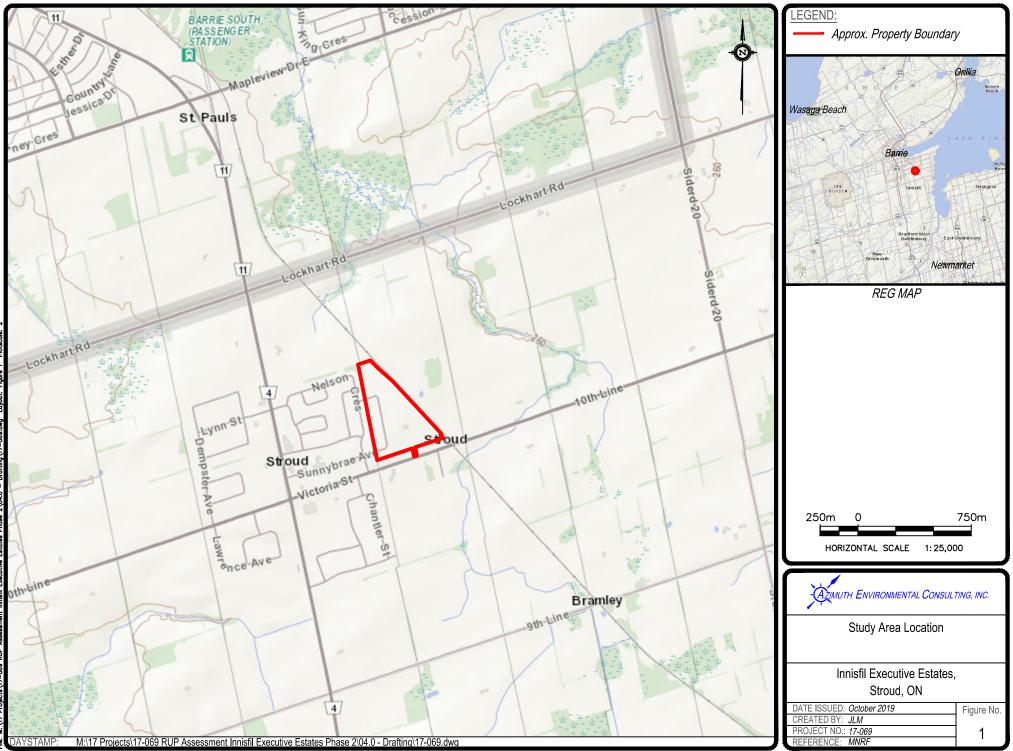
Appendix A: Figures Appendix B: Soils Information Appendix C: Water Balance Summary Appendix D: IEE Phase 1 Tertiary Treatment Permits



APPENDIX A

Figures

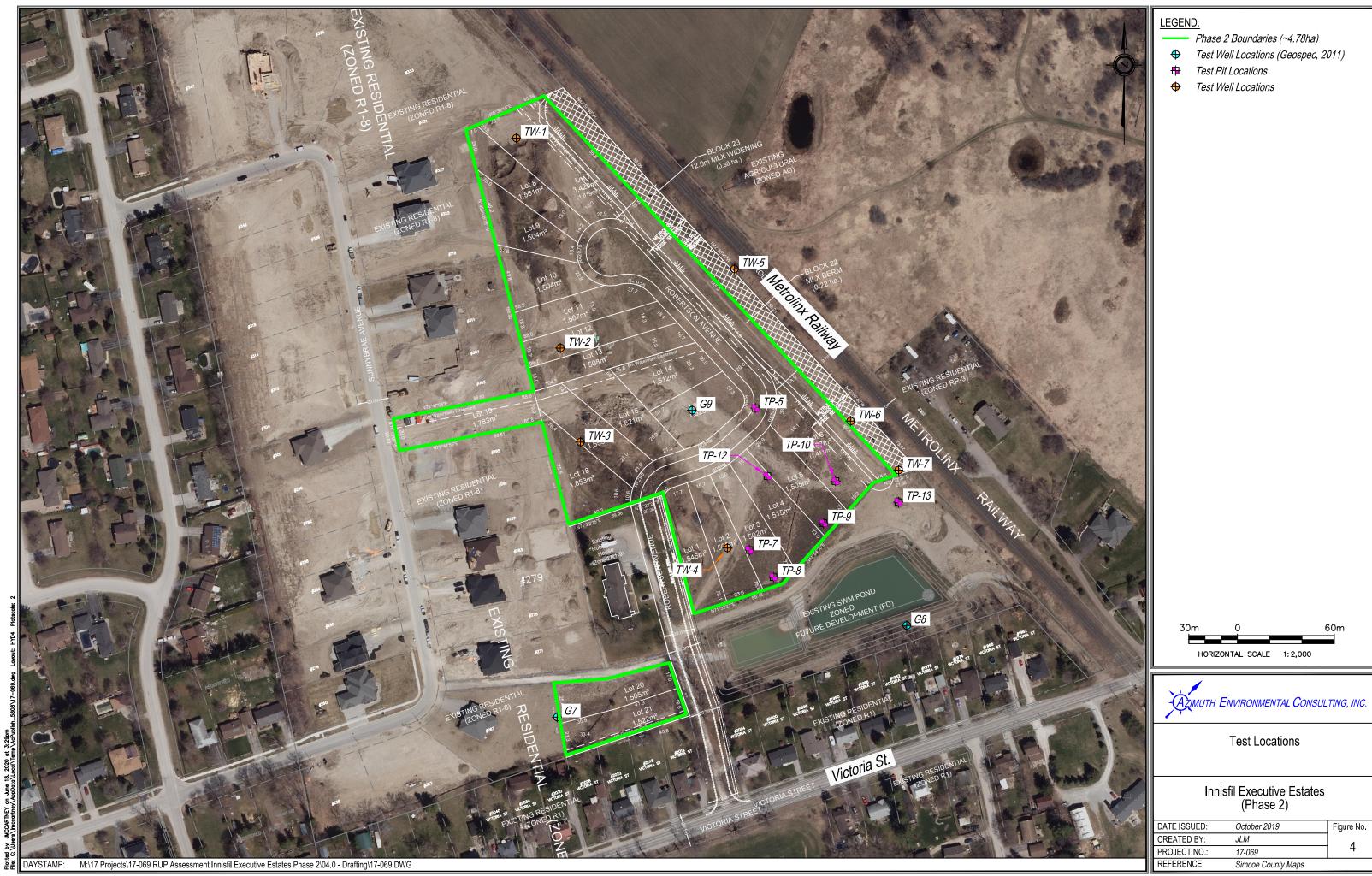
AZIMUTH ENVIRONMENTAL CONSULTING, INC.







by di



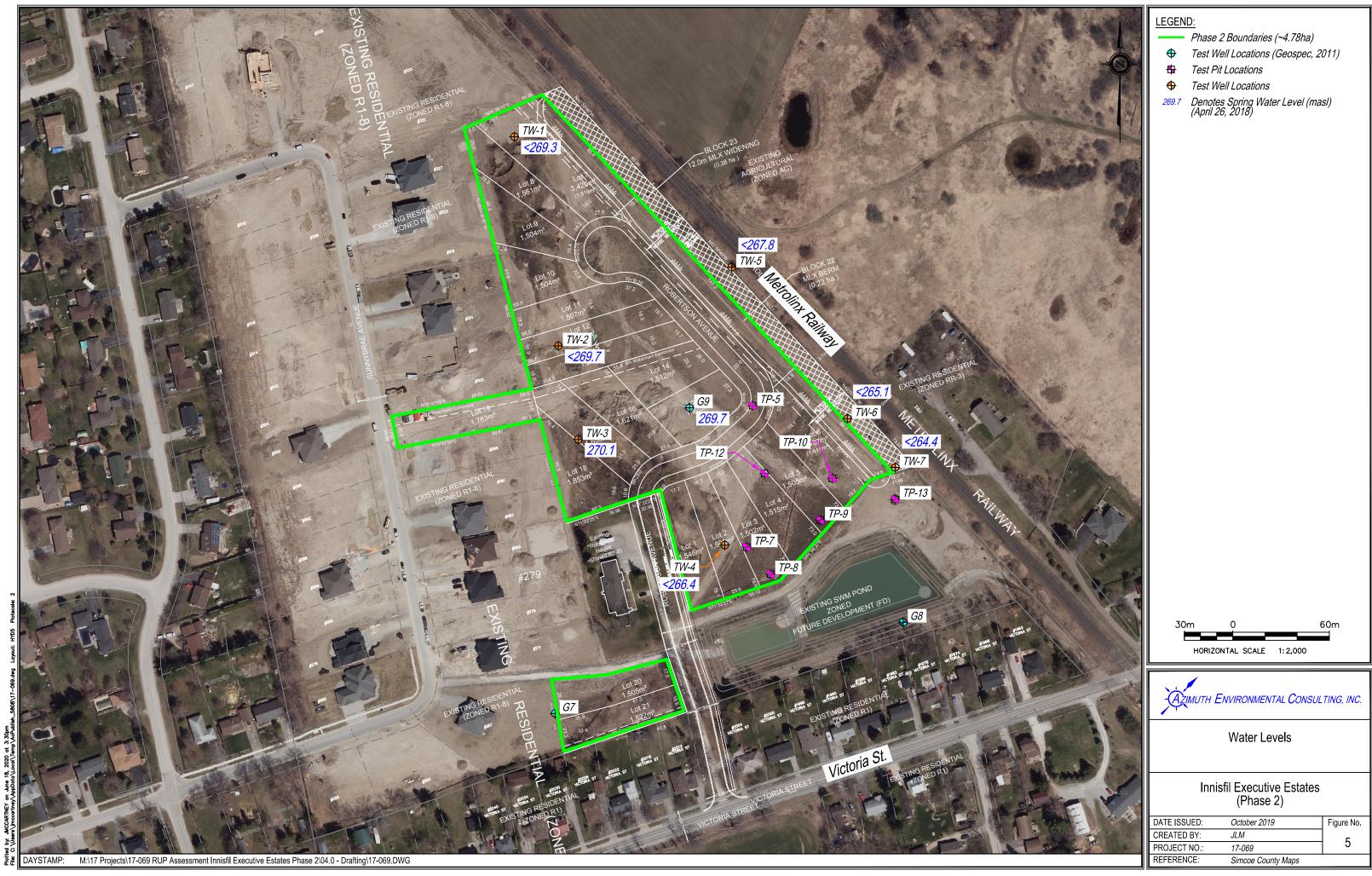
- Phase 2 Boundaries (~4.78ha)
- ✤ Test Well Locations (Geospec, 2011)

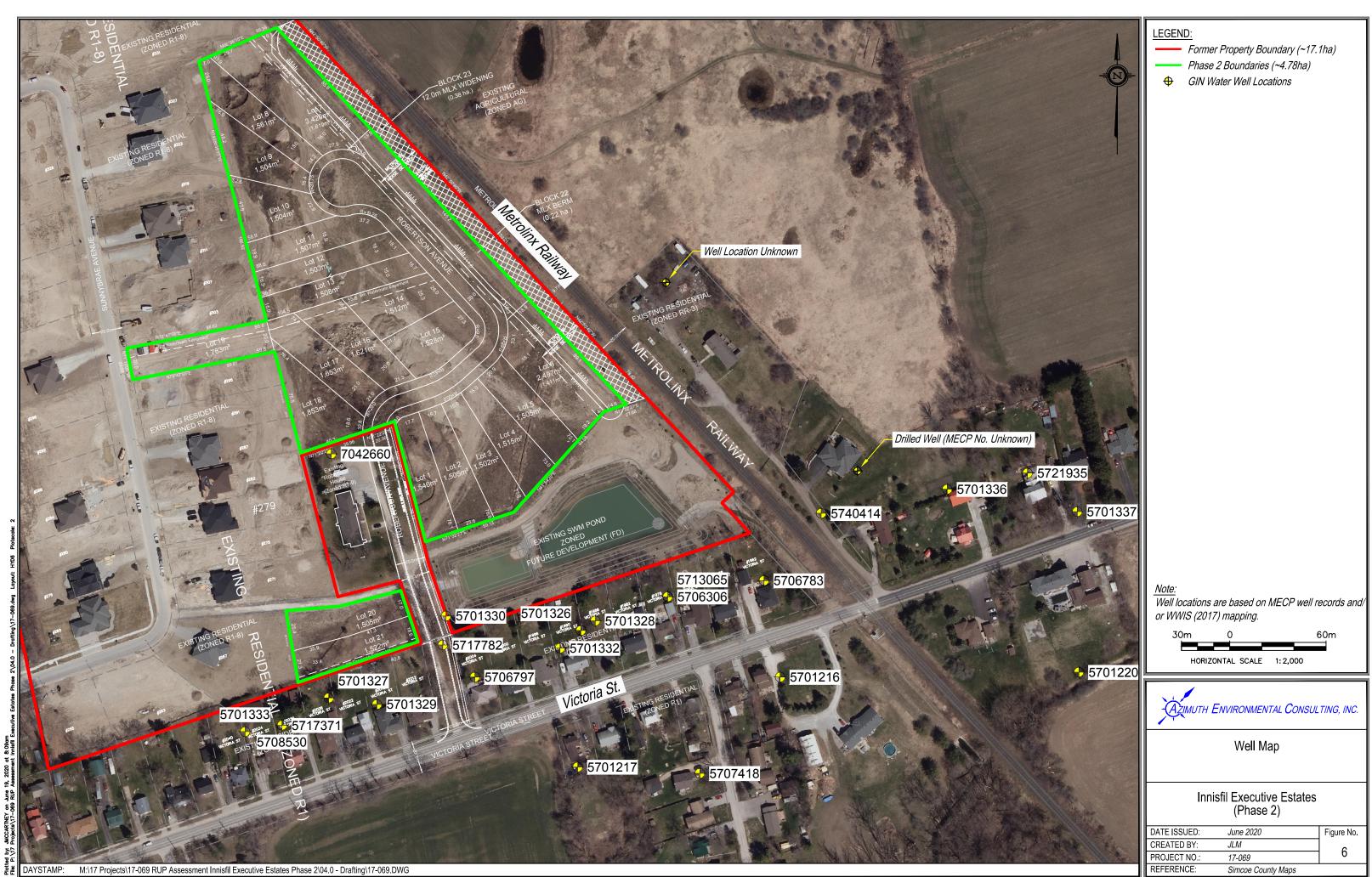
60m

Test Locations

Innisfil Executive Estates (Phase 2)

DATE ISSUED:	October 2019	Figure No.
CREATED BY:	JLM	
PROJECT NO .:	17-069	4
REFERENCE:	Simcoe County Maps	







APPENDIX B

Soils Information

AZIMUTH ENVIRONMENTAL CONSULTING, INC.



November 1, 2017

File No. 3-16-0041

Azimuth Environmental 642 Welham Road Barrie, ON L4N 9A1

Attention: Ms. Jackie Coughlin

ESTIMATION OF SOIL PERCOLATION RATE RE: SUBMITTED SOIL SAMPLES **PROJECT NO. 17-069**

Dear Sirs:

We are pleased to confirm the details of the estimation of soil percolation rate performed on the submitted soil samples for the above referenced project.

Terraprobe has performed a grain size distribution analysis on the four (4) soil samples delivered to our laboratory on October 13, 2017. The locations of delivered samples were identified as being from Project # 17-069.

Grain size distribution curves were plotted for the samples (Lab No. 1641a to 1641d). They are appended on the Wash Sieve and Sieve Hydrometer Analysis Test Report forms. Table 1 below represents a summary of the results of the samples tested.

Greater Toronto

11 Indell Lane Brampton, Ontario L6T 3Y3 (905) 796-2650 Fax 796-2250 brampton@terraprobe.ca

Hamilton - Niagara 903 Barton Street, Unit 22 Stoney Creek, Ontario L8E 5P5 (905) 643-7560 Fax 643-7559 stoneycreek@terraprobe.ca www.terraprobe.ca

Terraprobe Inc. **Central Ontario** 220 Bayview Drive, Unit 25 Barrie, Ontario L4N 4Y8 (705) 739-8355 Fax 739-8369 barrie@terraprobe.ca

Northern Ontario

1012 Kelly Lake Rd. Sudbury, Ontario P3E 5P4 (705) 670-0460 Fax 670-0558 sudbury@terraprobe.ca

Lab No.	Location of sample	Soil Description	Unified Soil Classification	Estimated Soil "T"-Time
1641a	TP 1 sa 1	Silty sand, some clay, trace gravel	SM	45 to 50 min/cm
1641b	TP 3 sa 2	Silty sand, trace clay, trace gravel	SM	40 to 45 min/cm
1641c	TP 4 sa 1	Gravelly sand, trace silt	SW-SP	4 to 6 min/cm
1641d	TP 6 sa 1	Silty sand, some clay, trace gravel	SM	40 to 45 min/cm

Table 1

It should be noted that Terraprobe Inc. did not conduct a field investigation in conjunction with the collection of these samples, or witness the collection of the samples tested. Terraprobe Inc. assumes no responsibility for the application of the above-noted percolation rates ("T"-Time) for use in design of an on-site sewage disposal system. The design of an on-site sewage system must be conducted by a qualified professional with due regard for a number of site-specific conditions in addition to the percolation rates of the soils.

Terraprobe Inc. does not present the estimated percolation rates given in this report as a warranty of performance for the soils tested. Furthermore, the estimate provided is indicative of the sample in a disturbed state only. It must be emphasized that factors such as, but not limited to, consistency, structure, organic content, density and degree of saturation could influence the estimate. The client or third party using this information as a basis for tile field design assumes all risk associated with their evaluation of this report and all other criteria used in the design of any private sewage disposal system.

We trust this information is sufficient for your present purposes. Should you have any questions concerning the content of the information presented, please do not hesitate to contact the undersigned.

Yours truly,

Terraprobe Inc.

Duguid. . Sc. T. Laboratory Manager

BHJ/jd Barrie Office

Brian H. Jackson Barrie Branch Manager



PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

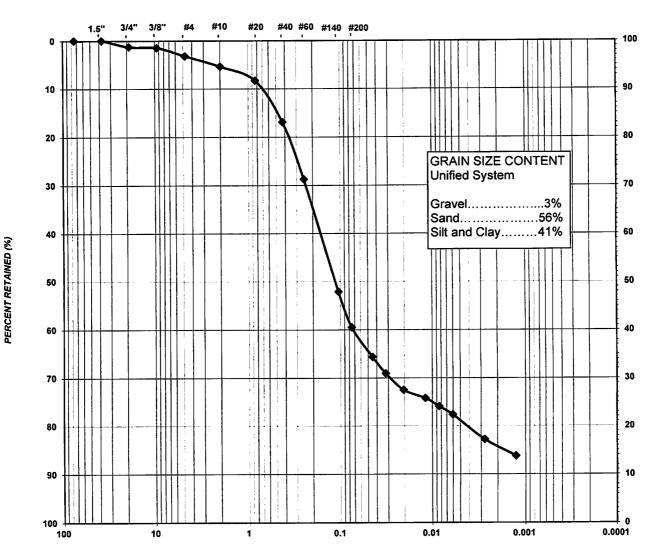
FILE NO.: 3-16-0041 LAB NO.: 1641a SAMPLE DATE: Oct-13-17 SAMPLED BY: Client

TEST PIT NUMBER: 1 SAMPLE DEPTH: 0.6 to 1.1m SAMPLE NUMBER: 1 SAMPLE LOCATION: Project No. 17-069 SAMPLE DESCRIPTION: Silty sand, some clay, trace gravel

Estimated Septic T-Time: 45 to 50 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GRAV	EL			AND	SILT	CLAY	
UNIFIED	COARSE	FINE	COARSE	MEDIUM	FINE	· · · · · · · · · · · · · · · · · · ·		
SYSTEM	GRAVEL			SAND	SAND SILT AND CLAY			



SIEVE AND HYDROMETER ANALYSIS TEST REPORT

PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

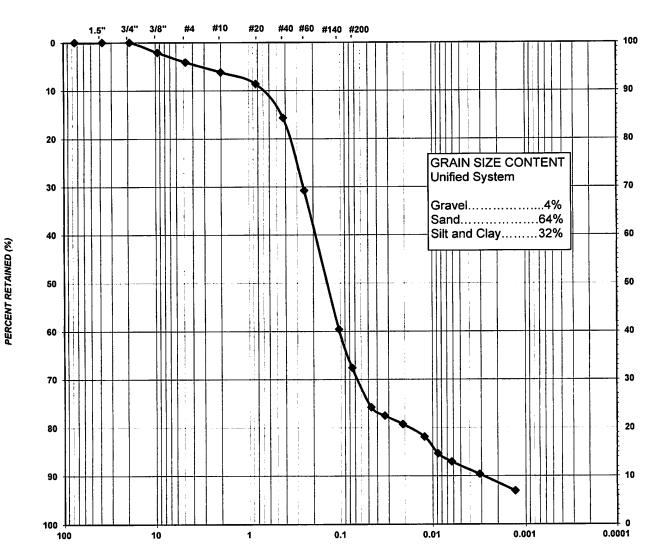
FILE NO.: 3-16-0041 LAB NO.: 1641b SAMPLE DATE: Oct-13-17 SAMPLED BY: Client

TEST PIT NUMBER: 3 SAMPLE DEPTH: 1.1m SAMPLE NUMBER: 2 SAMPLE LOCATION: Project No. 17-069 SAMPLE DESCRIPTION: Silty sand, trace clay, trace gravel

Estimated Septic T-Time: 40 to 45 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GRA	/EL				SILT	CLAY
UNIFIED	COARSE	FINE	COARSE	MEDIUM	FINE		
SYSTEM	GRAVEL			SAND		SILT AND CLAY	



PERCENT RETAINED (%)

WASH SIEVE ANALYSIS TEST REPORT

PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

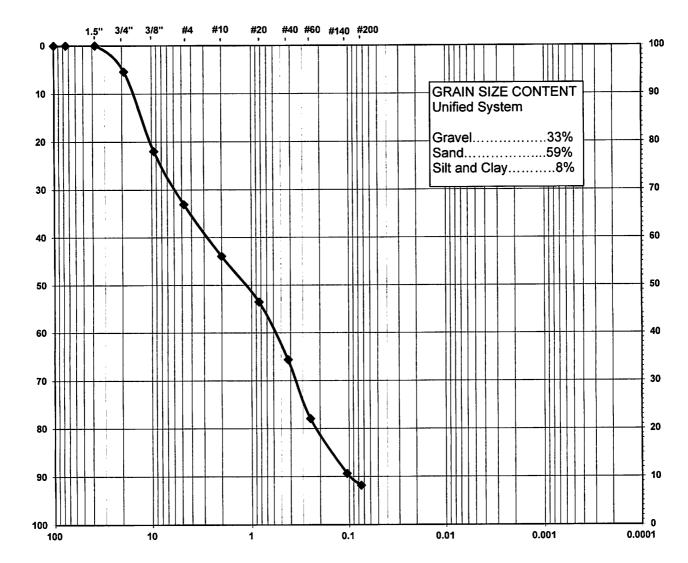
FILE NO.: 3-16-0041 LAB NO.: 1641c SAMPLE DATE: Oct-13-17 SAMPLED BY: Client

TEST PIT NUMBER: 4 SAMPLE DEPTH: 0.9 to 1.9m SAMPLE NUMBER: 1 SAMPLE LOCATION: Project No. 17-069 SAMPLE DESCRIPTION: Gravelly sand, trace silt

Estimated Septic T-Time: 4 to 6 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GR/	AVEL	-	COARSE MEDIUM FINE		SILT	CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE		
SYSTEM	GRAVE	VEL SAND		SILT AND CLAY			



SIEVE AND HYDROMETER ANALYSIS TEST REPORT

PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

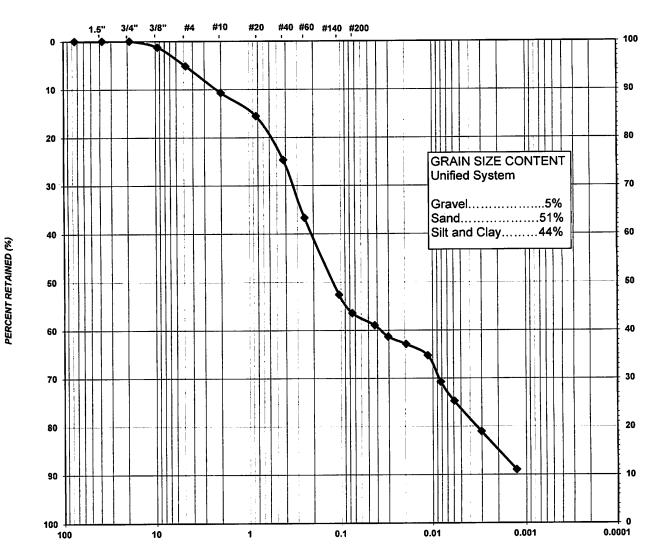
FILE NO.: 3-16-0041 LAB NO.: 1641d SAMPLE DATE: Oct-13-17 SAMPLED BY: Client

TEST PIT NUMBER: 6 SAMPLE DEPTH: 0.6 to 1.3m SAMPLE NUMBER: 1 SAMPLE LOCATION: Project No. 17-069 SAMPLE DESCRIPTION: Silty sand, trace clay, trace gravel

Estimated Septic T-Time: 40 to 45 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GRAVEL			COARSE MEDIUM FINE SAND		SILT	CLAY	
	COARSE	FINE	COARSE	MEDIUM	FINE	<u> </u>		
SYSTEM	GRAVEL		SAND			SILT AND CLAY		



March 16, 2018

File No. 3-16-0041

Azimuth Environmental 642 Welham Road Barrie, ON L4N 9A1

Attention: Ms. Jackie Coughlin, B.A.Sc., P. Eng.

RE: ESTIMATION OF SOIL PERCOLATION RATE SUBMITTED SOIL SAMPLES PROJECT NO. 17-069

Dear Ms. Coughlin:

We are pleased to confirm the details of the estimation of soil percolation rates performed on the submitted soil samples for the above referenced project.

Terraprobe has performed a grain size distribution analysis on the five (5) soil samples delivered to our laboratory on March 2, 2018. The locations of delivered samples were identified as being from Project # 17-069.

Grain size distribution curves were plotted for the samples (Lab No. 1905a to 1905e). They are appended on the Wash Sieve Analysis Test Report forms. Table 1 below represents a summary of the results of the samples tested.

Terraprobe Inc.

Greater Toronto 11 Indell Lane

Brampton, Ontario L6T 3Y3 (905) 796-2650 Fax 796-2250 brampton@terraprobe.ca Hamilton - NiagaraCentra903 Barton Street, Unit 22220 BayStoney Creek, Ontario L8E 5P5Barrie,(905) 643-7560 Fax 643-7559(705) 7stoneycreek@terraprobe.cabarrie@www.terraprobe.cawww.terraprobe.ca

Central Ontario 220 Bayview Drive, Unit 25 Barrie, Ontario L4N 4Y8 (705) 739-8355 Fax 739-8369 barrie@terraprobe.ca

Northern Ontario

1012 Kelly Lake Rd. Sudbury, Ontario P3E 5P4 (705) 670-0460 Fax 670-0558 sudbury@terraprobe.ca

Lab No.	Location of sample	Soil Description	Unified Soil Classification	Estimated Soil "T"-Time
1905a	TP 7	Sand, trace gravel, trace silt	SP	3 to 5 min/cm
1905b	TP 8	Sand and gravel, trace silt	SW-SP	2 to 4 min/cm
1905c	TP 10	Sand, trace gravel, trace silt	SP	4 to 6 min/cm
1905d	TP 11	Sand, some silt, some gravel	SW-SP	10 to 12 min/cm
1905e	TP 12	Sand, trace silt, trace gravel	SP	4 to 6 min/cm

Table 1

It should be noted that Terraprobe Inc. did not conduct a field investigation in conjunction with the collection of these samples, or witness the collection of the samples tested. Terraprobe Inc. assumes no responsibility for the application of the above-noted percolation rates ("T"-Time) for use in design of an on-site sewage disposal system. The design of an on-site sewage system must be conducted by a qualified professional with due regard for a number of site-specific conditions in addition to the percolation rates of the soils.

Terraprobe Inc. does not present the estimated percolation rates given in this report as a warranty of performance for the soils tested. Furthermore, the estimate provided is indicative of the sample in a disturbed state only. It must be emphasized that factors such as, but not limited to, consistency, structure, organic content, density and degree of saturation could influence the estimate. The client or third party using this information as a basis for tile field design assumes all risk associated with their evaluation of this report and all other criteria used in the design of any private sewage disposal system.

We trust this information is sufficient for your present purposes. Should you have any questions concerning the content of the information presented, please do not hesitate to contact the undersigned.

Yours truly,

Terraprobe Inc.

Jerry Duguid, A. Sc. T. Laboratory Manager

SG/jd Barrie Office

Steven Green, P. Eng.



WASH SIEVE ANALYSIS TEST REPORT

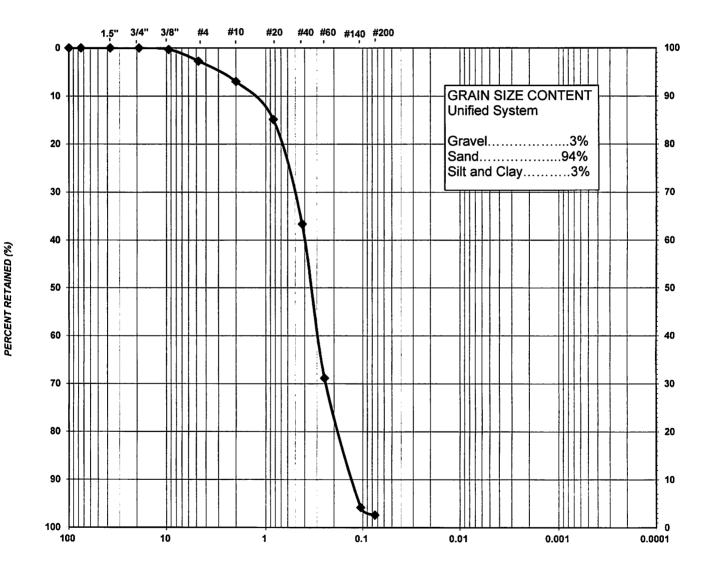
PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

TEST PIT NUMBER: 7 SAMPLE DEPTH: 6.0' SAMPLE NUMBER: 1 SAMPLE LOCATION: Project 17-069 SAMPLE DESCRIPTION: Sand, trace gravel, trace silt FILE NO.: 3-16-0041 LAB NO.: 1905a SAMPLE DATE: Mar-02-18 SAMPLED BY: Client

Estimated Septic T-Time: 3 to 5 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GR/	VEL				SILT CLAY	
UNIFIED			COARSE	MEDIUM FINE			
SYSTEM	SYSTEM GRAVEL			SAND		SILT AND CLAY	



WASH SIEVE ANALYSIS TEST REPORT

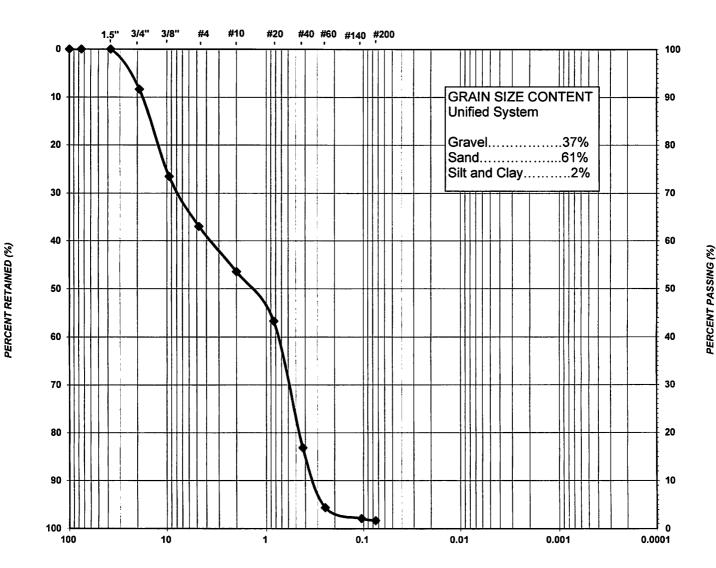
PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

TEST PIT NUMBER: 8 SAMPLE DEPTH: 6.0' SAMPLE NUMBER: 1 SAMPLE LOCATION: Project 17-069 SAMPLE DESCRIPTION: Sand and gravel, trace silt FILE NO.: 3-16-0041 LAB NO.: 1905b SAMPLE DATE: Mar-02-18 SAMPLED BY: Client

Estimated Septic T-Time: 2 to 4 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

UNIFIED COARSE FINE COARSE MEDIUM FINE	MIT SYSTEM	GRA	VEL	-	 MEDIUM FINE	SILT	CLAY
SYSTEM GRAVEL SAND SILT AND CLAY	UNIFIED SYSTEM			COARSE	 1	SILT AND CLAY	





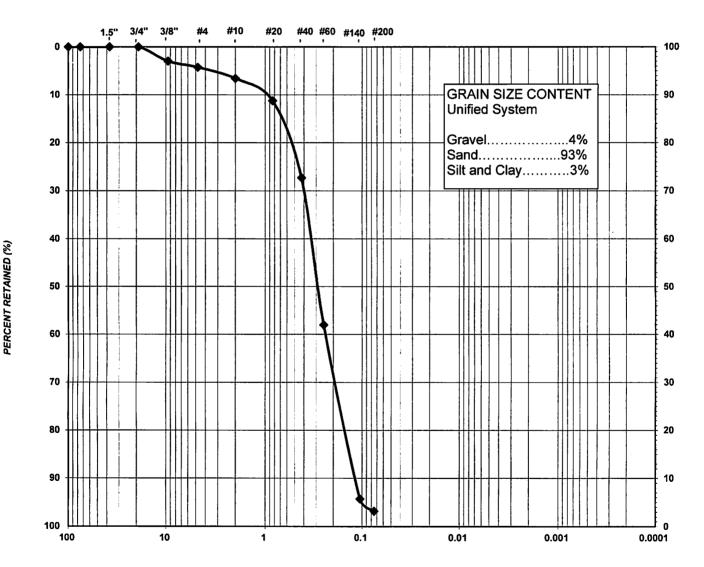
PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

TEST PIT NUMBER: 10 SAMPLE DEPTH: 6.0' SAMPLE NUMBER: 1 SAMPLE LOCATION: Project 17-069 SAMPLE DESCRIPTION: Sand, trace gravel, trace silt FILE NO.: 3-16-0041 LAB NO.: 1905c SAMPLE DATE: Mar-02-18 SAMPLED BY: Client

Estimated Septic T-Time: 4 to 6 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GRA	VEL		COARSE MEDIUM FINE		SILT CLAY	
UNIFIED	D COARSE FINE COA		COARSE	E MEDIUM FINE			
SYSTEM	GRAVEL			SAND		SILT AND CLAY	

PERCENT PASSING (%)



PERCENT RETAINED (%)



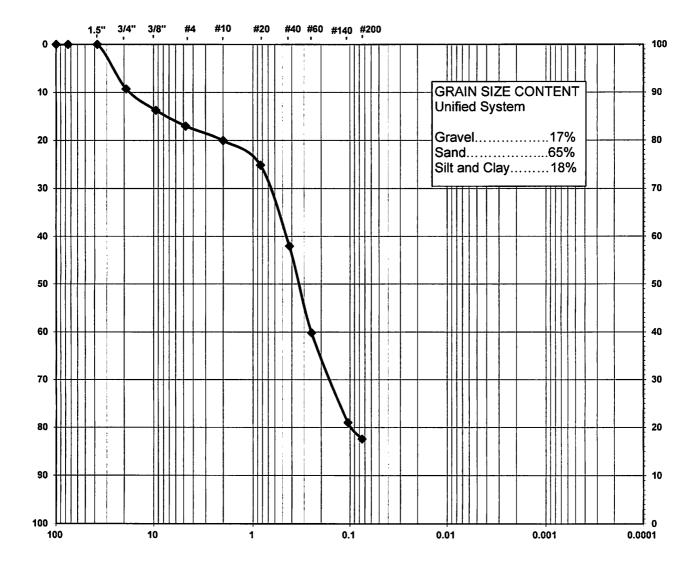
PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

TEST PIT NUMBER: 11 SAMPLE DEPTH: 3.0' SAMPLE NUMBER: 1 SAMPLE LOCATION: Project 17-069 SAMPLE DESCRIPTION: Sand, some silt, some gravel FILE NO.: 3-16-0041 LAB NO.: 1905d SAMPLE DATE: Mar-02-18 SAMPLED BY: Client

Estimated Septic T-Time: 10 to 12 min/cm

GRAIN SIZE DISTRIBUTION

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GRA	VEL		COARSE MEDIUM FINE		SILT	CLAY
UNIFIED			COARSE	MEDIUM FINE		·]
SYSTEM	GRAVEL			SAND		SILT AND CLAY	

PERCENT PASSING (%)



TEST PIT NUMBER: 12

SAMPLE NUMBER: 1

SAMPLE LOCATION: Project 17-069

SAMPLE DESCRIPTION: Sand, trace silt, trace gravel



PROJECT: Laboratory Testing; Septic T-Time LOCATION: N/G CLIENT: Azimuth Environmental

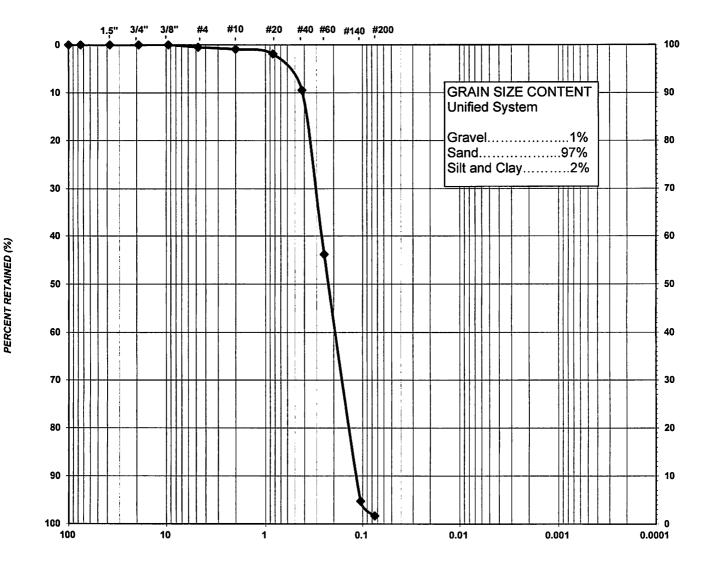
FILE NO.: 3-16-0041 LAB NO.: 1905e SAMPLE DATE: Mar-02-18 SAMPLED BY: Client

Estimated Septic T-Time: 4 to 6 min/cm

GRAIN SIZE DISTRIBUTION

SAMPLE DEPTH: 4.0 to 5.5'

U.S. STANDARD SIEVE SIZES



GRAIN SIZE (mm)

MIT SYSTEM	GRA	VEL		COARSE MEDIUM FINE		SILT CLAY	
UNIFIED SYSTEM			COARSE	DARSE MEDIUM FINE		SILT AND CLAY	

PERCENT PASSING (%)



APPENDIX C

Water Balance Summary

Table A: Pre-Development

· · · · ·			
Catchment Designation	Meadow	Total	
Area (m ²)	47,800	47,800	
Pervious Area (m ²)	47,800	47,800	
Impervious Area (m ²)	0	0	
Infiltration Factors			
Topography Infiltration Factor	0.2		
Soil Infiltration Factor	0.3		
Land Cover Infiltration Factor	0.15		
Infiltration Factor	0.65		
Run-Off Coefficient	0.35		
Run-Off From Impervious Surfaces	0.8		
Inputs (Per Unit Area)			
Precipitation (mm/yr)	908	908	
Rainfall (mm/yr)	655	655	
Run-On (mm/yr)	0	0	
Other Inputs (mm/yr)	0	0	
Total Inputs (mm/yr)	908	908	
Outputs (Per Unit Area)			
Precipitation Surplus (mm/yr)	424	424	
Net Surplus (mm/yr)	424	424	
Evapotranspiration (mm/yr)	484	484	
Infiltration (mm/yr)	276	276	
Surplus Infiltration (mm/yr)	0	0	
Total Infiltration (mm/yr)	276	276	
Run-Off Pervious Areas (mm/yr)	148	148	
Run-Off Impervious Areas (mm/yr)	0	0	
Total Run-Off (mm/yr)	148	148	
Total Outputs (mm/yr)	908	908	
Difference (Inputs - Outputs)	0	0	
Inputs (Volumes)		1	
Precipitation (m ³ /yr)	43,402	43,402	
Run-On (m ³ /yr)	0	0	
Other Inputs (m ³ /yr)	0	0	
Total Inputs (m ³ /yr)	43,402	43,402	
Outputs (Volumes)			
Precipitation Surplus (m ³ /yr)	20,267	20,267	
Net Surplus (m ³ /yr)	20,267	20,267	
Evapotranspiration (m ³ /yr)	23,135	23,135	
Infiltration (m ³ /yr)	13,174	13,174	
Surplus Infiltration (m ³ /yr)	0	0	
Total Infiltration (m ³ /yr)	13,174	13,174	
Run-Off Pervious Areas (m ³ /yr)	7,094	7,094	
Run-Off Impervious Areas (m ³ /yr)	0	0	
Total Run-Off (m ³ /yr)	-	-	
	7,094	7,094	
Total Outputs (m ³ /yr)	43,402	43,402	
Difference (Inputs - Outputs)	0	0	

Table B: Post-Development (no mit)

		T			
					Total
39,322	1,320	/	540	4,180	47,800
39,322	0	0	0	0	39,322
0	1,320	2,438	540	4,180	8,478
0.2	0	0	0	0	
0.3	0	0	0	0	
0.1	0	0	0	0	
0.6	0	0	0	0	
-					
0.8	0.8	0.8	0.8	0.8	
908	908	908	908	908	908
655	655	655	655	655	655
0	0	0	0	0	0
0		0	0	0	0
908	908	908	908	908	908
424	726	726	726	726	478
424	726	726	726	726	478
484	182	182	182	182	430
254	0	0	0	0	209
0	0	0	0	0	0
254	0	0	0	0	209
170	0	0	0		140
-					129
170	726	726	726	726	268
908	908	908	908	908	908
0	0	0	0	0	0
35,704	1,199	2,214	490	3,795	43,402
0	0	0	0	0	0
0	0	0	0	0	0
35 704	1 100	2 21/	100	3 705	43,402
33,704	1,133	2,214	430	5,755	43,402
10.072	050	4 774	202	2.020	00.004
,		,		,	22,831
,		/			22,831
,					20,571
,	-	-	-		10,004
0	0	0	0	0	0
10,004	0	0	0	0	10,004
6,669	0	0	0	0	6,669
0	959	1,771	392	3,036	6,158
				, ·	,
6.669	959	1.771	392	3.036	12.827
6,669 35,704	959 1,199	1,771 2,214	392 490	3,036 3,795	12,827 43,402
	0.2 0.3 0.1 0.6 0.4 0.8 908 655 0 0 0 908 424 424 424 424 424 424 424 424 424 42	Landscaped Grass Driveway 39,322 1,320 39,322 0 0 1,320 0 1,320 0 1,320 0 1,320 0.2 0 0.3 0 0.4 1 0.8 0.8 908 908 655 655 0 0 0 0 908 908 424 726 424 726 424 726 484 182 254 0 0 0 254 0 0 726 170 726 908 908 0 0 0 0 0 0 170 726 908 908 0 0 0 0 0 0	39,322 $1,320$ $2,438$ $39,322$ 0 0 0 $1,320$ $2,438$ 0.2 0 0 0.3 0 0 0.4 1 1 0.8 0.8 0.8 0.4 1 1 0.8 0.8 0.8 908 908 908 655 655 655 0 0 0 0 0 0 0 0 0 908 908 908 908 908 908 424 726 726 424 726 726 424 726 726 484 182 182 254 0 0 0 726 726 170 726 726 908 908 908 0 0 0 <t< td=""><td>39,322 1,320 2,438 540 $39,322$ 0 0 0 0 0 1,320 2,438 540 0 1,320 2,438 540 0 0 0 0 0 0.1 0 0 0 0 0.6 0 0 0 0 0.4 1 1 1 1 0.8 0.8 0.8 0.8 0.8 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 9</td><td>39,322 $1,320$ $2,438$ 540 $4,180$ $39,322$ 0 0 0 0 0 0 $1,320$ $2,438$ 540 $4,180$ 0.2 0 0 0 0 0 0.3 0 0 0 0 0 0.4 1 0 0 0 0 0.4 1 1 1 1 1 0.8 0.8 0.8 0.8 0.8 0.8 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908</td></t<>	39,322 1,320 2,438 540 $39,322$ 0 0 0 0 0 1,320 2,438 540 0 1,320 2,438 540 0 0 0 0 0 0.1 0 0 0 0 0.6 0 0 0 0 0.4 1 1 1 1 0.8 0.8 0.8 0.8 0.8 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 9	39,322 $1,320$ $2,438$ 540 $4,180$ $39,322$ 0 0 0 0 0 0 $1,320$ $2,438$ 540 $4,180$ 0.2 0 0 0 0 0 0.3 0 0 0 0 0 0.4 1 0 0 0 0 0.4 1 1 1 1 1 0.8 0.8 0.8 0.8 0.8 0.8 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908 908

18%

Table C: Post-Development (with mitigation)

•						
Catchment Designation	Landscaped Grass	Driveway	Roads	Sidewalk	Structure	Total
Area (m²)	39,322	1,320	2,438	540	4,180	47,800
Pervious Area (m ²)	39,322	0	0	0	0	39,322
Impervious Area (m ²)	0	1,320	2,438	540	4,180	8,478
Infiltration Factors						
Topography Infiltration Factor	0.2	0	0	0	0	
Soil Infiltration Factor	0.3	0	0	0	0	
Land Cover Infiltration Factor	0.1	0	0	0	0	
Infiltration Factor	0.6	0	0	0	0	
Run-Off Coefficient	0.4	1	1	1	1	
Run-Off From Impervious Surfaces	0.8	0.8	0.8	0.8	0.8	
Inputs (Per Unit Area)						
Precipitation (mm/yr)	908	908	908	908	908	908
Rainfall (mm/yr)	655	655	655	655	655	655
Run-On (mm/yr)	0	0	0	0	0	0
Other Inputs (mm/yr)	0	0	0	0	0	0
Total Inputs (mm/yr)	908	908	908	908	908	908
Outputs (Per Unit Area)						
Precipitation Surplus (mm/yr)	424	726	726	726	726	478
Net Surplus (mm/yr)	424	726	726	726	726	478
Evapotranspiration (mm/yr)	484	182	182	182	182	430
Infiltration (mm/yr)	254	0	0	0	0	209
Surplus Infiltration (mm/yr)	47	0	0	0	314	66
Total Infiltration (mm/yr)	302	0	0	0	314	276
Run-Off Pervious Areas (mm/yr)	122	0	0	0	0	101
Run-Off Impervious Areas (mm/yr)	0	726	726	726	412	101
Total Run-Off (mm/yr)	122	726	726	726	412	202
Total Outputs (mm/yr)	908	908	908	908	908	908
Difference (Inputs - Outputs)	0	0	0	0	0	0
Inputs (Volumes)						
Precipitation (m ³ /yr)	35,704	1,199	2,214	490	3,795	43,402
Run-On (m³/yr)	0	0	0	0	0	0
Other Inputs (m ³ /yr)	0	0	0	0	0	0
Total Inputs (m ³ /yr)	35,704	1,199	2,214	490	3,795	43,402
Outputs (Volumes)		,	,		-/	-, -
Precipitation Surplus (m ³ /yr)	16,673	959	1,771	392	3,036	22,831
Net Surplus (m ³ /yr)	16,673	959	1,771	392	3,036	22,831
Evapotranspiration (m ³ /yr)	19,032	240	443	98	759	20,571
Infiltration (m ³ /yr)	10,004	0	0	98	0	10.004
Surplus Infiltration (m ³ /yr)	, ,	0	-	-	-	- /
	1,856		0	0	1,314	3,170
Total Infiltration (m ³ /yr)	11,860	0	0	0	1,314	13,174
Run-Off Pervious Areas (m ³ /yr)	4,813	0	0	0	0	4,813
Run-Off Impervious Areas (m ³ /yr)	0	959	1,771	392	1,722	4,844
Total Run-Off (m ³ /yr)	4,813	959	1,771	392	1,722	9,657
Total Outputs (m ³ /yr)	35,704	1,199	2,214	490	3,795	43,402
Difference (Inputs - Outputs)	0	0	0	0	0	0

	Site						
Characteristic	Pre- Development	Post- Development	Change (Pre to Post)		Post-Development with Mitigation	Change (Pre to Post with Mitigation)	
			Inputs (Vol	ume)		-	
Precipitation (m ³ /yr)	43,402	43,402	0	0%	43,402	0	0%
Run-On (m ³ /yr)	0	0	0	NA	0	0	NA
Other Inputs (m ³ /yr)	0	0	0	NA	0	0	NA
Total Inputs (m ³ /yr)	43,402	43,402	0	0%	43,402	0	0%
			Outputs (Vo	lume)		-	
Precipitation Surplus (m ³ /yr)	20,267	22,831	2,564	13%	22,831	2,564	13%
Net Surplus (m3/yr)	20,267	22,831	2,564	13%	22,831	2,564	13%
Evapotranspiration (m ³ /yr)	23,135	20,571	-2,564	-11%	20,571	-2,564	-11%
Infiltration (m ³ /yr)	13,174	10,004	-3,170	-24%	10,004	-3,170	-24%
Rooftop Infiltration (m ³ /yr)	0	0	0	NA	3,170	3,170	NA
Total Infiltration (m ³ /yr)	13,174	10,004	-3,170	-24%	13,174	0	0%
Run-Off Pervious Areas (m ³ /yr)	7,094	6,669	-425	-6%	4,813	-2,281	-32%
Run-Off Impervious Areas (m ³ /yr)	0	6,158	6,158	NA	4,844	4,844	NA
Total Run-Off (m ³ /yr)	7,094	12,827	5,734	81%	9,657	2,564	36%
Total Outputs (m ³ /yr)	43,402	43,402	0	0%	43,402	0	0%

Table D: Water Balance Summary Table



APPENDIX D

IEE Phase 1 Tertiary Treatment Permits

Lot 4 (335 Sunnybrae Ave.) Building Permit No.: 2018-0203 https://moar.innisfil.ca/buildingPermit/PrintPermit/2018-0203

BUILDING PERMIT

Number: 2018-0203

Schedule a Building Inspection:

Please book your inspection(s) online by clicking this link: www.innisfil.ca/eservices or Email: buildinginspections@innisfil.ca or Leave a phone message at: 705-436-3710 Ext. 3500

Applicant : Owner : Legal Description : Roll Number : Lou Kelly Lou Kelly PLAN 51M1045 LOT 4 010035054140000

Inspections Required:

- Sewage System Readiness to Construct
- Sewage System Substantial Completion
- Notice of Completion

Conditions/Remarks:

Install new septic system for SFD

Water-Loo Wire mesh basket Septic system

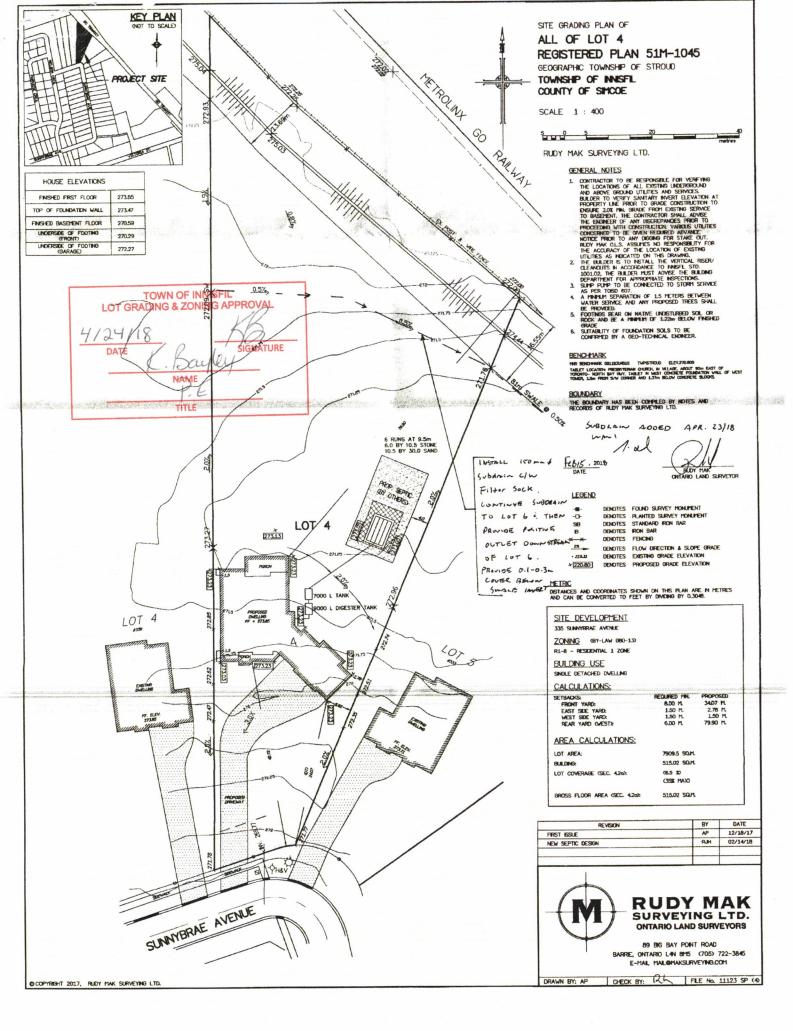
Maintenance contract required for Water-Loo Treatment system

Ensure header and distribution piping is able to be detected magnetically via 14 gauge tracer wire or other means.

Ensure distribution piping and septic tank are minimum distance from all well and property lines.

Page 2 of 2

WASER-LOO WIRE SUSSEM WASER-LOO SEPTIC SUSSEM BUSKET SEPTIC



or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor. Toronto, M5G 2E5 (416) 585-6666.



Schedule 1: Designer Information

Use one form for each individual who reviews and takes responsibility for design activities with respect to the project.

A. Project Infor	mation				
Building number, st	reet name			Unit no.	Lot/con.
Municipality			Plan number/ other desc	and the second se	1
B. Individual w	ho reviews and ta	kes respons	sibility for design act	ivities	
Name Jason Ches	ock	na manan manan (ananan sasan (na na n	Firm Rumball Excavation		Ta areas
Street address 408	Tiffin Street,		1	Unit no.	Lot/con.
Municipality Barrie		L4N 5W8	Province ON	E-mail jschesloc	k@gmail.com
Telephone number		Fax number (705) 735-	1701	Cell number (705) 623-3	889
(705)722-114 C Design activ	ities undertaken	ov individua	i identified in Section	n B. [Building C	ode Table
3.5.2.1. of Divisi	on C]			Building S	A REAL PROPERTY AND A REAL
 House Small Bui Large Bui Complex 	ldings Buildings	🗖 Buildi		Plumbing Plumbing	- House
Description of desi D. Declaration	of Designer				
	son Cheslock	un adres son daare er daar verste vlade daar og boons ve	declare that (choose one as app	ropriate):
·00		name)			
3.2.4 class	1.of Division C, of the ses/categories.	Building Cod	design work on behalf of e. I am qualified, and the	Inthi is registered, i	der subsection n the appropriate
	Firm BCIN:	_15632			
L l rev desi	gner" under subsecti Individual BCIN:	on 3.2.5.07 Dr	design and am qualified i vision C, of the Building C ion:	Joue.	ategory as an "othe
	design work is exern Basis for exemption qualification:	npt from the re from registrat	gistration and qualificatio	on requirements of t	he Building Code.
I certify that: 1. The info 2. I have s	ubmitted this applica	this schedule tion with the k	is true to the best of my nowledge and consent of	knowledge. f the firm.	hesioner
February 7,	2018 Date		The		
NOTE	na an a	ana na mangana sana na karanggan ana yana na sana na sana na karangan ana	(

1.For the purposes of this form, "individual" means the "person" referred to in Clause 3.2.4.7(1) d) of Division C, Article 3.2.5.1. of Division C, and all other persons who are exempt from qualification under Subsections 3.2.4. and 3.2.5. of Division C. Application for a Permit to Construct or Demolish – Effective January 1, 2011

2. Schedule 1 is not required to be completed by a holder of a license, temporary license, or a certificate of practice, issued by the Ontario Association of Architects. Schedule 1 is also not required to be completed by a holder of a license to practise, a limited license to practise, or a certificate of authorization, issued by the Association of Professional Engineers of Ontarlo.

Schedule 2: Sewage System Installer Information

A. Project Information Building number, street name			Unit number	Lot/con.
<u> </u>	Postal code	Plan number/ othe		Loodon
Municipality	Postal code	Fian number our		مىلىدەت ھەتتەتلەت كەتتە ، بەتەك بۇر قىرۇ قىلىتە، ئۇلارىدا، بۇت 10- تو بىلەتچە" بۇر. مۇر بىلە بەت سەتتەت
Sewage system installer				
s the installer of the sewage syste cleaning or emptying sewage syste Yes (Continue to Section	ems, in accordar C) No (Continu	nce with Building Coo le to Section E)	le Article 3.3.1.1, Div Installer unkno (Continue to S	wn at time of application
Registered installer informat		swer to B is "Yes"		ungalah mengerakanakan kanana mela di mengeran di pada ana kanangan menananan ang menghagan kanan kanan menan
Name Rumball Excavation and Ha	aulage		BCIN 10457	
Street address 408 Tiffin Street			Unit number	Lot/con.
Municipality Barrie	Postal code L4N 5W8	Province ON		ock@gmail.com
Telephone number	Fax (705)735-	1701	Cell number (705) 62	3-3889
(705) 722-1145 Qualified supervisor informa	tion (where an	swer to section I		
Name of qualified supervisor(s)			fication Number (BC	CIN)
Name of qualitied supervisor(s)				
J Cheslock		10457	ana e quadhani sabulari muras manar antaran semara ma manana mana mana a da disebu	ar alayan gana a ana a ana a ana a ana a ana an
R Cheslock		10456		
Declaration of Applicant:				naar aan waxaa ahaa ahaa ahaa ahaa ahaa ahaa aha
	son Cheslock		de	eclare that:
(print r	name)			
I am the applicant for the application, I shall subrease application, I shall subrease application.	ne permit to cons mit a new Schedu	truct the sewage sys ule 2 prior to construc	stem. If the installer ction when the instal	is unknown at time of ler is known;
OR				
I am the holder of the p that the installer is know		ot the sewage system	n, and am submitting	a new Schedule 2, now
I certify that:				
	d in this cohodu	la is true to the hest	of my knowledge	
2. If the owner is a corpora	tion or partnersh	ip, I have the authori	- 1	
January 7, 2018 D	ate	q.	Signature	of applicant

Lot 5 (333 Sunnybrae Ave.) Building Permit No.: 2016-1177

Jackie Coughlin

From:	Online Building Inspections [moar@innisfil.ca]
Sent:	Monday, June 10, 2019 3:36 PM
To:	Sigmund
Subject:	Innisfil Building Permit Inspection - Permit 2016-1177

Application Number2016-1177 Address 333 SUNNYBRAE AVE Owner(s): 1820839 ONTARIO INC Legal description of Property: PLAN 51M1045 LOT 5 Roll Number 010035054150000

Inspected by Todd McCulloch on 2019-06-10 **Inspection Type** Sewage System - Substantial Completion **Inspection Status** Acceptable with o/s deficiencies

Inspection Comments Maintenance contract required Alarm test required As built drawing required for area change

Tanks not installed at time of inspection

Ok to cover bed area

CAUTION You are required to book an inspection when the corrections have been made. Acceptance and approval by a building inspector is required. Construction may not be concealed until the above infractions have been inspected by the Town of Innisfil and accepted by the building inspector. Failure to resolve the outstanding concerns listed above may result in the issuance of an Order, including a Stop Work Order.

Rumball Excavation & Haulage

408 Tiffin St Barrie, Ontario L4N 9W8 (705) 722-1145 Fax (705) 735-1701

February 3, 2019

ANT - IEE Remington A, Lot 5, Revised Waterloo Baskets

- 1. "T" of original controlling soil layer 40 min/cm
- 2. Total "fixture units" value for all dwelling units: 31.5
- 3. Total number of bedrooms in all dwelling units: 4
- 4. Total finished floor area in all dwelling units: 327 square meters
- 5. Total daily design sanitary sewage flow: 3300 liters per day
- 6. Minimum septic tank size 7000 liters
- 7. Calculations:

A – is the area in m2 Q – is the daily design sanitary sewage flow in liters T – is the percolation times of the underlying native soil in min/cm to a max of 50

<u>Stone Area</u> A = Q/50A = 3300/50 A= 66 m²

Sand Area $A = Q \times T/850$ A = (3300x 40)/400 $A = 330 m^2$

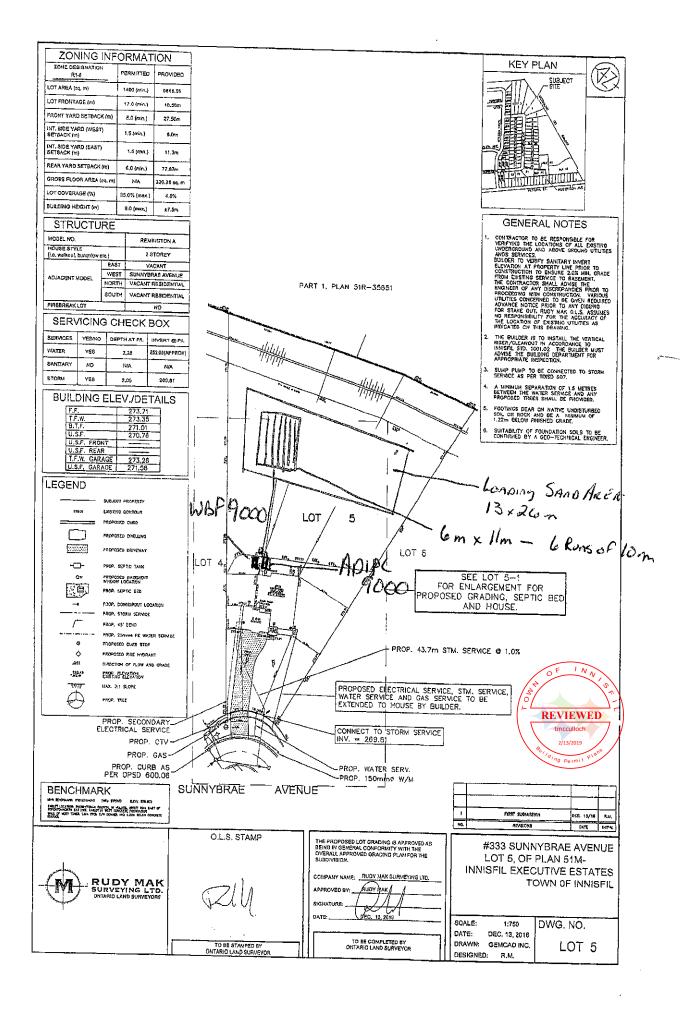
Stone Area	66
Sand Area	3

66 m² 330 m²

8. Benchmark established as original grade



BCIN Authorization #. 10457 Signature:



Lot 6 (331 Sunnybrae Ave.) Building Permit No.: 2017-0701

Jackie Coughlin

From:	Peter Slusarczyk [moarinnisfil@gmail.com]
Sent:	Friday, January 25, 2019 8:20 AM
То:	Sigmund
Subject:	Innisfil Building Permit Inspection - Permit 2017-0701

Application Number2017-0701 Address 331 SUNNYBRAE AVE Owner(s): EZEKIEL TRACY LYNN Legal description of Property: PLAN 51M1045 LOT 6 Roll Number 010035054160000

Inspected by Peter Slusarczyk on 2019-01-25 00:00:00.000 **Inspection Type** Sewage System - Substantial Completion **Inspection Status** Acceptable with o/s deficiencies

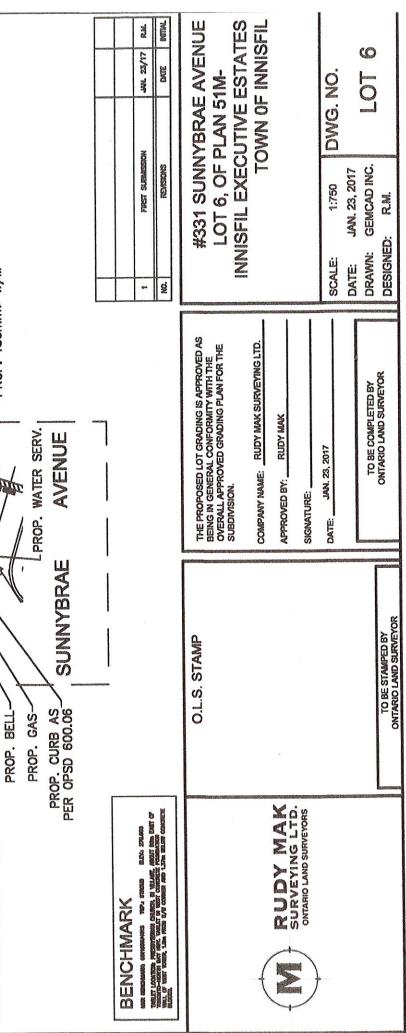
Inspection Comments

-Maintenance contract received. -Alarm test conducted. -As built received.

Call for Final inspection when erosion control in place.

CAUTION You are required to book an inspection when the corrections have been made. Acceptance and approval by a building inspector is required. Construction may not be concealed until the above infractions have been inspected by the Town of Innisfil and accepted by the building inspector. Failure to resolve the outstanding concerns listed above may result in the issuance of an Order, including a Stop Work Order.

KEY PLAN			世代							GENERAL NOTES	1. CONTRACTOR TO BE RESPONSIBLE FOR VERFANG THE LOCATIONS OF ALL EXSTING IMMERGROUND AND ABOVE GROUND UTILITIES	ANDS SERVICES. BUILDER TO VERIFY SANITARY INVERT ELEVATION AT PROPERTY LINE PRIOR TO	CONSTRUCTION TO ENSURE 2.05 MIN. GRADE FROM EDGTING SERVICE TO BASEMENT. THE CONTRACTOR SHALL ADVISE THE	ENGINEER OF ANT DISCREPANALES FROM ID PROCEEDING WITH CONSTRUCTION. VARIOUS UTILITIES CONCERNED TO BE GVEN REQUIRED	ADVANCE NUMER FINISH TO ANT MAGNING FOR STAKE OUT. RUDY MAK OLLS. ASSUMES NO RESPONSIBILITY FOR THE ACUTAGY OF THE LOCATION OF ENGINE ITH THES AS		A THE DUILDER IS TO INSTALL THE VERTICAL RISER/CLEANOUT IN ACCORDANCE TO INNESTL STD. 1001.02 THE BUILDER MUST ADVISST THE DUIL DEPARTMENT FOR	APPROPRIATE INSPECTION.		4. A MINIMUM SEPARATION OF 1.5 METRES BETWEEN THE WATER SERVICE AND ANY PROPOSED TREES SHALL BE PROVIDED.	5. FOOTINGS BEAR ON NATIVE UNDISTURBED SOIL OR ROCK AND BE A MINIMUM OF	ئە مە	× 10m	2		SEE LOT 6-1 INLARGEMENT FOR	GRADING, AND HOUS	o Digeske Tavic)					PROPOSED ELECTRICAL SERVICE, SIM. SERVICE, WATER SERVICE AND GAS SERVICE TO BE EXTENDED TO HOUSE BY BUILDER.		m SIM. SERVICE @ 1.0%	O STORM SERVICE	ONDARY	M/W M/W
												PART 1, PLAN 51R-35651		THE			100 mm m		Saus MACA	10m × 30m					and conteres		TZM RPROPOSED	1350		del tion	skets.			WATER SER		43.7m	CONNECT TO STORM	PROP. SECONDARY	LL PROP. 150mmø W/W
ZONING INFORMATION	ZONE DESIGNATION PERMITTED PROVIDED R1-3	LOT AREA (sq. m) 1400 (min.) 6868.55	LOT FRONTAGE (m) 17.0 (min.) 18.58m	FRONT VARD SETBACK (m) 8.0 (min.) 25.02m	INT. @IDE YARD (WEST) 1.5 (min.) 4.32m SETBACK (m)	INT. SIDE YARD (EAST) 1.5 (min.) 4.25m SETBACK (m)	REAR YARD SETBACK (m) 6.0 (min.) 82.70m	V (sq. m) N/A 34:	35.0% (max.)	BUILDING HEIGHT (m) 9.0 (max.) 6.05m	TURE	MODEL NO. BUNGALOW BUNGALOW	EAST EAST SIN	ADJACENT MODEL NORTH VACANT RESIDENTIAL	SOUTH VACANT RESIDENTIAL FIREBREAK LOT NO	SFRVICING CHECK BOX	SERVICES YESMO DEPTHAT PL INVERT @ PL	YES 2.28	ON VO	STORM YES 2.05 269.60	BUILDING ELEV./DETAILS	F.F. 273.52 T.F.W 273.16	270.51 Hm		T.F.W. GARAGE 273.07 U.S.F. GARAGE 271.39		ALLEGEL PROPERTY	INDER CONTOUR	PROPOSED DWELLING	PROPOSED DRIVEWAY		OW PROPOSED BASEMENT WINDOW LOCATION FROM SEPTIC RED	G.	PROP. STORM SERVICE	PROP. 25mms P		ARE DIRECTION OF FLOW AND GRADE		PROP. BEL



Lot 13 (303 Sunnybrae Ave.) Building Permit No.: 2018-0871

BUILDING PERMIT

Number: 2018-0871

Schedule a Building Inspection:

Please book your inspection(s) online by clicking this link: <u>www.innisfil.ca/eservices</u> or Email: buildinginspections@innisfil.ca or Leave a phone message at: 705-436-3710 Ext. 3500

Applicant : Owner : Legal Description : Roll Number :

Sigmund Tronowicz, Ant Construction 1820839 ONTARIO INC PLAN 51M1045 LOT 13 010035054230000

Inspections Required:

- Sewage System Readiness to Construct
- Sewage System Substantial Completion
- Notice of Completion

Conditions/Remarks:

New Septic Installation

WATER_LOO Wire mesh basket

-Maintenance agreement required

-As built required

-Provide granular analysis for native and imported soil prior to install inspection.

-Ensure header and distribution piping is able to be detected magnetically via 14 gauge tracer wire or other means.

-Ensure distribution piping and septic tank are minimum distance from all wells and property lines

Page 2 of 2



Project Location : 303 SUNNYBRAE AVE

Work Type : Septic

ATTENTION :

- Owner/agent is required to arrange for all required site inspections as listed on this permit. Book your Inspection online at www.innisfil.ca/eservices two business days in advance of the preferred date of inspection.
 Owner/agent is also required to be aware of the list of inspections and notes to this permit indicated on the next page(s) and also be aware of any notes/marks in red on the attached plans and/or documents.
 All plans and/or documents attached to this permit form part of this permit and are to remain on site and available to the Inspector.
 Owner/agent is required to comply with the Ontario Building Code and any other applicable
- Owner/agent is required to comply with the Ontario Building Code and any other applicable law at all times.

0EC-17-2018 for Chief Building Official (signature) Date

Community Development Standards Branch Town of Innisfil 2101 Innisfil Beach Rd Innisfil, ON L9S 1A1 705-436-3710 888-436-3710 www.innisfil.ca

Jackie Coughlin

From:	Online Building Inspections [moar@innisfil.ca]
Sent: To:	Thursday, September 19, 2019 4:12 PM Sigmund
Subject:	Innisfil Building Permit Inspection - Permit 2018-0871

Application Number2018-0871 Address 303 SUNNYBRAE AVE Owner(s): 1820839 ONTARIO INC Legal description of Property: PLAN 51M1045 LOT 13 Roll Number 010035054230000

Inspected by Todd McCulloch on 2019-09-19 **Inspection Type** Sewage System - Substantial Completion **Inspection Status** Acceptable with o/s deficiencies

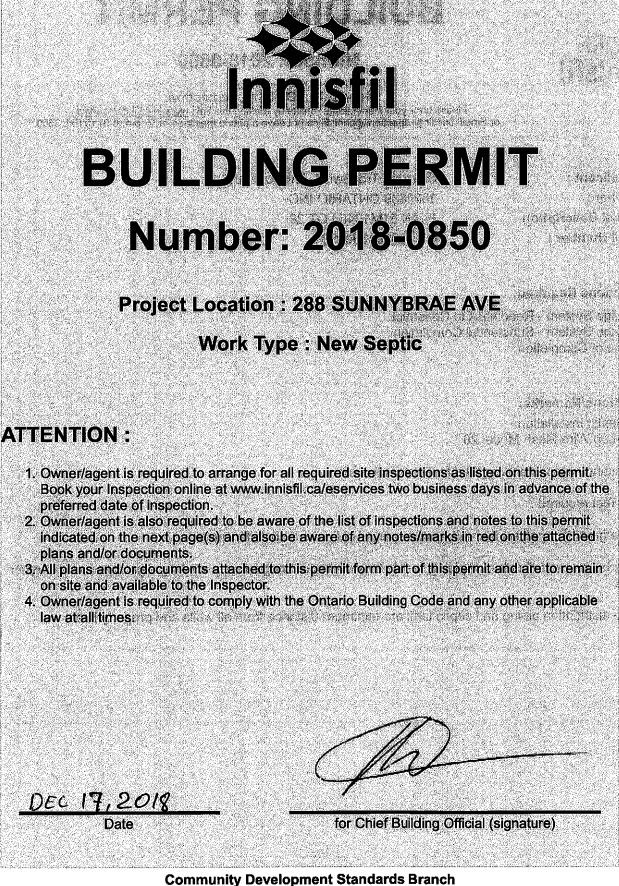
Inspection Comments Maintenance contract required Alarm test required As built required Appears as per approved drawings

Tanks not hooked to house at time of inspection

Ok to cover

CAUTION You are required to book an inspection when the corrections have been made. Acceptance and approval by a building inspector is required. Construction may not be concealed until the above infractions have been inspected by the Town of Innisfil and accepted by the building inspector. Failure to resolve the outstanding concerns listed above may result in the issuance of an Order, including a Stop Work Order.

Lot 14 (288 Sunnybrae Ave.) Building Permit No.: 2018-0850



Community Development Standards Branch Town of Innisfil 2101 Innisfil Beach Rd Innisfil, ON L9S 1A1 705-436-3710 888-436-3710 www.innisfil.ca

Jackie Coughlin

From:	Moar Automation [moar@innisfil.ca]
Sent:	Thursday, December 5, 2019 3:48 PM
То:	Sigmund
Subject:	Innisfil Building Permit Inspection - Permit 2017-0651

Application Number2017-0651 Address 295 SUNNYBRAE AVE Owner(s): 1820839 ONTARIO INC Legal description of Property: PLAN 51M1045 LOT 14 Roll Number 010035054240000

Inspected by Ryan Dobie on 2019-12-05 **Inspection Type** Sewage System - Substantial Completion **Inspection Status** Acceptable with o/s deficiencies

Inspection Comments

Setbacks appear to comply to OBC Appears as per approved drawings Alarm test required Maintenance contract required

Ok to cover

CAUTION You are required to book an inspection when the corrections have been made. Acceptance and approval by a building inspector is required. Construction may not be concealed until the above infractions have been inspected by the Town of Innisfil and accepted by the building inspector. Failure to resolve the outstanding concerns listed above may result in the issuance of an Order, including a Stop Work Order.

Lot 23 (255 Sunnybrae Ave.) Building Permit No.: 2019-0202



BUILDING PERMIT Number: 2019-0202

Project Location : 255 SUNNYBRAE AVE

Work Type : Septic

ATTENTION :

- 1. Owner/agent is required to arrange for all required site inspections as listed on this permit. Book your Inspection online at www.innisfil.ca/eservices two business days in advance of the preferred date of inspection.
- 2. Owner/agent is also required to be aware of the list of inspections and notes to this permit indicated on the next page(s) and also be aware of any notes/marks in red on the attached plans and/or documents.
- 3. All plans and/or documents attached to this permit form part of this permit and are to remain on site and available to the Inspector.
- 4. Owner/agent is required to comply with the Ontario Building Code and any other applicable law at all times.

June 11, 2019

Date

for Chief Building Official (signature)

Community Development Standards Branch

Town of Innisfil 2101 Innisfil Beach Rd Innisfil, ON L9S 1A1 705-436-3710 888-436-3710 www.innisfil.ca

Page 1 of 2

BUILDING PERMIT

Number: 2019-0202

Schedule a Building Inspection:

Please book your inspection(s) online by clicking this link: <u>www.innisfil.ca/eservices</u> or Email: buildinginspections@innisfil.ca or Leave a phone message at: 705-436-3710 Ext. 3500

Applicant : Owner : Legal Description : Roll Number :

Jason Cheslock, Rumball Excavation 1820839 ONTARIO INC PLAN 51M1045 LOT 23 010035054330000

Inspections Required:

- Sewage System Readiness to Construct
- Sewage System Substantial Completion
- Notice of Completion

Conditions/Remarks:

New Septic Installation Water-Loo Biofilter Basket BA-30

-Maintenance agreement required for treatment system

-Ensure header and distribution piping is able to be detected magnetically via 14 gauge tracer wire or other means.

-Ensure distribution piping and septic tank are minimum distance from all wells.

Page 2 of 2

Rumball Excavation & Haulage 408 Tiffin Street Barrie, Ontario L4N 9W8 (705) 722-1145

February 25, 2019

Lauren Kelley Residence Waterloo Baskets Model BA30

- 1. "T" of original controlling soil layer 50 min/cm
- 2. Total "fixture units" value for all dwelling units: 31
- 3. Total number of bedrooms in all dwelling units: 4
- 4. Total finished floor area in all dwelling units: 243 square meters
- 5. Total daily design sanitary sewage flow: 2550 liters per day
- 6. Calculations:

A – is the area in m2 Q – is the daily design sanitary sewage flow in liters T – is the percolation times of the underlying native soil in min/cm to a max of 50

Stone Laver	Sand Laver
A = Q/75	$A = Q \times T/400$
A = 2550/75	A = (2550 x 50)/400
A= 34 m ²	$A = 320 \text{ m}^2$

Minimum Stone layer Area – 34 m² to a minimum depth of 250 mm Minimum Sand layer Area – 320 m² to minimum depth of 250 mm

BCIN Authorization #. 10457 Signature:

Rumball Excavation & Haulage

408 Tiffin St Barrie, Ontario L4N 9W8 (705) 722-1145 Fax (705) 735-1701

February 25, 2019

IEE, Lauren Kelley Residence

Total Daily Design Sanitary Sewage Flow Rate Calculations

Fixture Count	Units
Basement 1 – 3 piece	6
Main Floor Kitchen Sink Dishwasher Laundry Tub Washer 1 - 4 piece 1 - 3 Piece	1.5 1.5 1.5 1.5 7.5 6
1 - 2 piece	5.5

TOTAL 31

4 Bedrooms - 2000 L/D Fixture Count 31 = 550 L/D 243 m² = 500 L/D Q = 2550 T = 50



Town of Innisfil

Do Not C	omplete
Permit No	Frank - Marken and -
Revision	No.

Date___

Schedule 3 **Proposed Services**

2. Water supply D Proposed Z Existing

4. Type of Well Dug/bored/Sandpoint well

Drilled well

Municipal

C Other

6. Sewage Design Flow for Other Occupancies Design Flow L/day Detailed sewage flow calculations:

🛛 Class 4 – Area Bed

C Fully raised

Z Partially raised

□ In-ground

Class 4 - Acrobic with Trench

Fully raised

C Partially raised

🗆 In-ground

Class 4 - Aerobic with Filter Media

C Fully raised

Partially raised

🗆 In-ground

Class 5 - Holding Tank

1. Engineered OYes

O No

3. Type of work proposed Z New Installation

C Replacement

□ Alteration

5. Residential Sewage Design Flow Info. Bedrooms House (floor area) People Total Fixture Units 31 Residential Flow 2557

m (Schedule 7) L/day

7. Type of System

□ Treatment Unit ____

□ Class 2 - Leaching Pit

Class 3 - Cesspool

□ Class 4 – Shallow Buried Trench

- 🗆 Class 4 Trench
 - □ Fully raised
 - C Partially raised
 - □ In-ground

🗆 Class 4 - Filter Media

I Fully raised

D Partially raised

In-ground



Schedule 4 Sewage System Details

lete

Type of System WATCHLOO Bof. 1kg	(Schedule 4)
Septic/Holding Tank 6135 L	and an and a second
Septic Tank Effluent Filter Digeolog tow	k
Treatment Unit - Make & Model WArckLoo	
Number of Units	μ_{μ} μ_{μ} μ_{μ} χ_{μ}
Refer to Typical Drawing	Pump(s) required 40
Mantle Information:	Pump Rate / CC L/15min
Native or imported =15m indirection(s)	Note: Alarm required for all
	pumping systems
Slope subgrade% slope	
/ directi	on(s)
θ Trench	6 Shallow Buried Trench
Distribution Pipe Length m	Pipe Length m
Loading Aream ²	······································
Type of Chamber	0 Filter Media Bed
Length of Chamber m	Stone m ²
Area Bed	Extended Base m ²
Stone <u>34</u> m ²	Pipe m
Sand <u>320</u> m ²	Weight of Filter Media Kg
Pipe <u>30m</u> m	Loading Aream ²
Construction Notes: BASE Cut 600mm	
	1999 - 199

Version 04/06

Do Not Con	nplete
Permit No_	
Revision No	
Date	



Schedule 6 Fixture unit count

Fixtures	# Existing	x + #	[‡] Proposed	X	unit count	-	Fixture Count
Bathroom							
Bathroom group (toilet, sink and tub or shower) with flush tank		-jan	3	x	6	and a second	18
Bathtub with/without overhead shower		÷-	1	X	1.5		1.5
Shower stall		÷		Х	1.5	dense mana	
Wash basin (1½inch trap)		- to	1	Х	1.5	anista anista	1.5
Watercloset (toilet) tank operated		+	1	X	4	Antonioupy, antonio dennia	4
Bidet		+		X	and the second se	onenn Meine	
Kitchen						, in family of the	
Dishwasher		+)	X	1	steens Right)
Sink with/without garbage grinder(s), domestic and other small type single, double or 2 single with a common trap				X	1.5	Segment down	1.5
Other							
Domestic washing machine		+	/	X	1.5	1000	1.5
Combination sink and laundry tray single or double (Installed on 1½ trap)		na se investe intereste antereste se	1	X	1.5	2004 3004	
Insert the TOTAL in section 5 of Schodule 4 (0	Mohamatana ang mangga mang mang				1	otal	: 30.5

Insert the TOTAL in section 5 of Schedule 4 (0.Reb.403/97 Table 7.4.9.3)

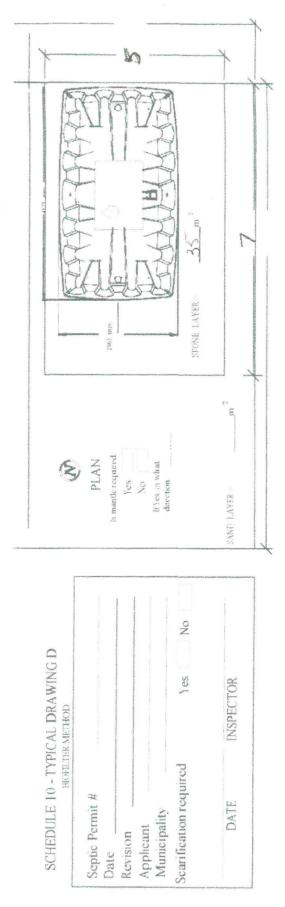
- 1. Sump pumps and floor drains are not to be connected to the sewage system. Connection of such fixtures to a sewage system may lead to a hydraulic failure of the said system. The above mentioned fixtures should be discharged separately to an approved Class 2 (leaching pit) sewage system.
- 2. Where laundry waste is not more than 20% of the total daily design sanitary sewage flow, it may discharge to a sewage system (Part 8, OBC, 8.1.3.1(2)).

FEB 25 2019

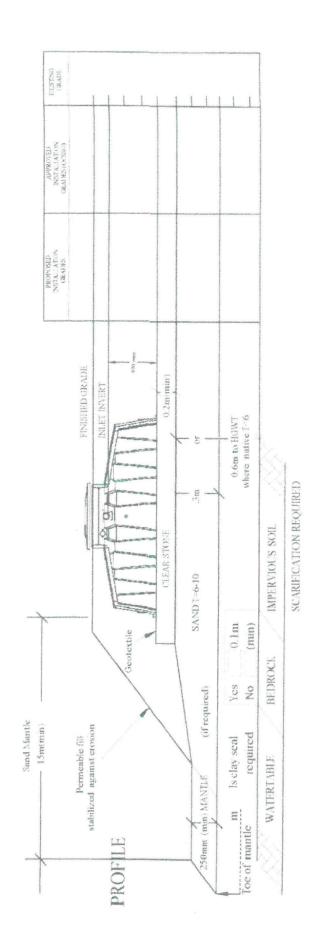
Agend Owner signature

Date





NOT TO SCALE



Lot 26 (255 Sunnybrae Ave.) Building Permit No.: 2018-0921



BUILDING PERMIT Number: 2018-0921

Project Location : 280 SUNNYBRAE AVE

Work Type : Septic

ATTENTION :

- 1. Owner/agent is required to arrange for all required site inspections as listed on this permit. Book your Inspection online at www.innisfil.ca/eservices two business days in advance of the preferred date of inspection.
- 2. Owner/agent is also required to be aware of the list of inspections and notes to this permit indicated on the next page(s) and also be aware of any notes/marks in red on the attached plans and/or documents.
- 3. All plans and/or documents attached to this permit form part of this permit and are to remain on site and available to the Inspector.
- 4. Owner/agent is required to comply with the Ontario Building Code and any other applicable law at all times.

December 21, 2018

Date

for Chief Building Official (signature)

Community Development Standards Branch

Town of Innisfil 2101 Innisfil Beach Rd Innisfil, ON L9S 1A1 705-436-3710 888-436-3710 www.innisfil.ca

Page 1 of 2

BUILDING PERMIT

Number: 2018-0921

Schedule a Building Inspection:

Please book your inspection(s) online by clicking this link: <u>www.innisfil.ca/eservices</u> or Email: buildinginspections@innisfil.ca or Leave a phone message at: 705-436-3710 Ext. 3500

Applicant : Owner : Legal Description : Roll Number :

Andrea Kelly 1820839 ONTARIO INC PLAN 51M1045 LOT 26 010035054360000

Inspections Required:

- Sewage System Readiness to Construct
- Sewage System Substantial Completion
- Notice of Completion

Conditions/Remarks:

New Septic Installation for new SFD

Water-Loo Treatment system

Maintenance agreement required

Ensure header and distribution piping is able to be detected magnetically via 14 gauge tracer wire or other means.

Ensure distribution piping and septic tank are minimum distance from all wells and property lines

Page 2 of 2

Rumball Excavation & Haulage

408 Tiffin St Barrie, Ontario L4N 9W8 (705) 722-1145 Fax (705) 735-1701

November 27, 2018

ANT - IEE, Lot 26, Sunnybrae, The Belcourt A

- 1. "T" of original controlling soil layer 50 min/cm
- 2. Total "fixture units" value for all dwelling units: 32
- 3. Total number of bedrooms in all dwelling units: 4
- 4. Total finished floor area in all dwelling units: 272 square meters
- 5. Total daily design sanitary sewage flow: 2800 liters per day
- 6. Minimum septic tank size 6150 liters
- 7. Calculations: A - is the area in m2 Q - is the daily design sanitary sewage flow in liters T - is the percolation times of the underlying native soil in min/cm to a max of 50

Stone Area	Sand Area
A = Q/75	$A = Q \times T/400$
A =2800/75	A = (2800x 50)/400
A= 38 m²	$A = 350 \text{ m}^2$

Minimum Stone Area	38 m²
Minimum Sand Area	350 m²

8. Benchmark established as original grade

Loading Rates for fill based absorption trenches and filter beds

Table 8.7.4.1.A

BCIN Authorization #. 10457

Signature:

Rumball Excavation & Haulage

408 Tiffin St Barrie, Ontario L4N 9W8 (705) 722-1145 Fax (705) 735-1701

November 27, 2018

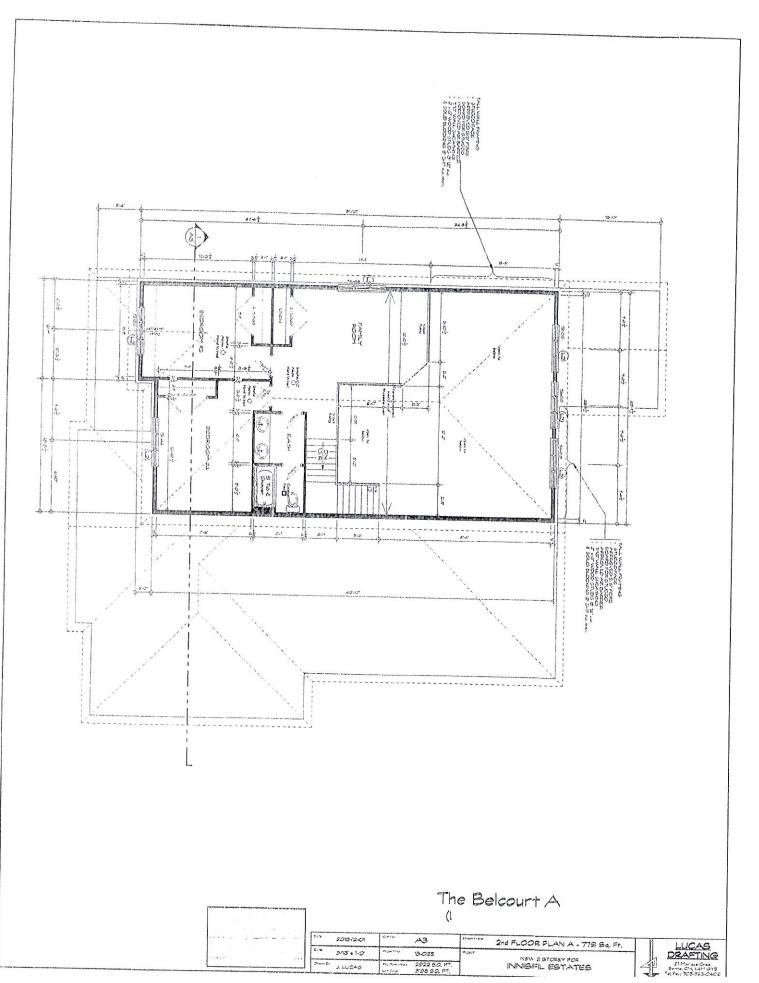
ANT - IEE, Lot 26, Sunnybrae, The Belcourt A

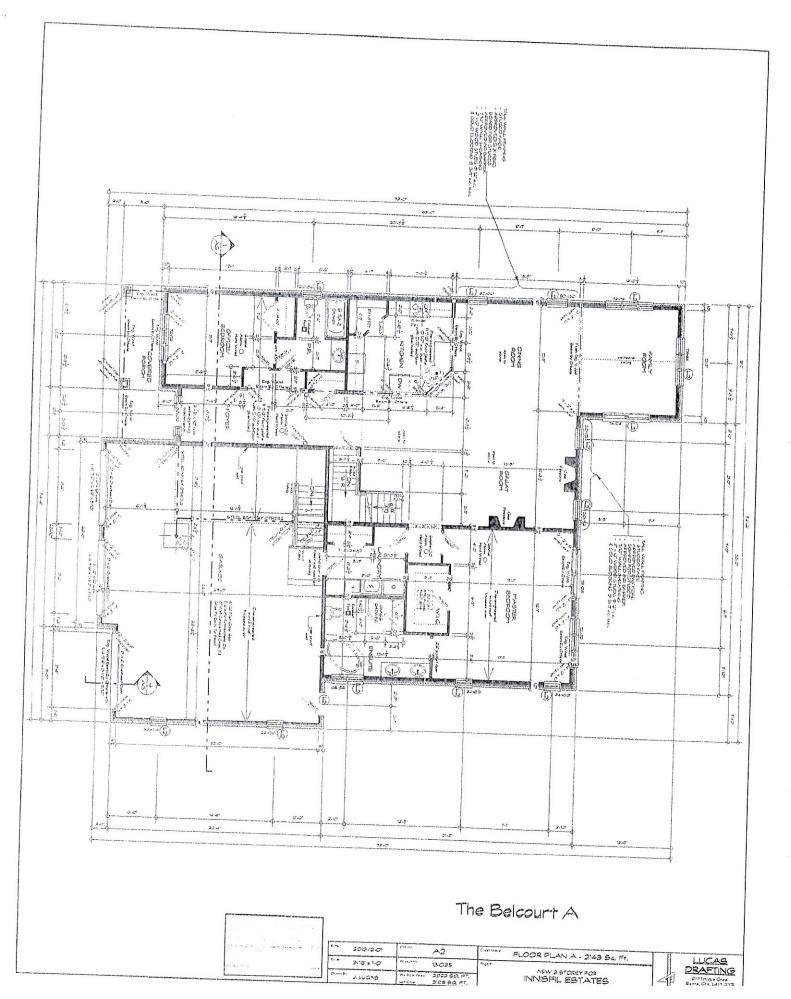
Total Daily Design Sanitary Sewage Flow Rate Calculations

Fixture Count	Units
Basement 1 – 3 piece	6
Main Floor Kitchen Sink Dishwasher Laundry Tub Washer Bidet 1 - 4 piece 1 - 2 piece	1.5 1.5 1.5 1.5 1 7.5 5.5
Second Floor 1 – 3 piece	6

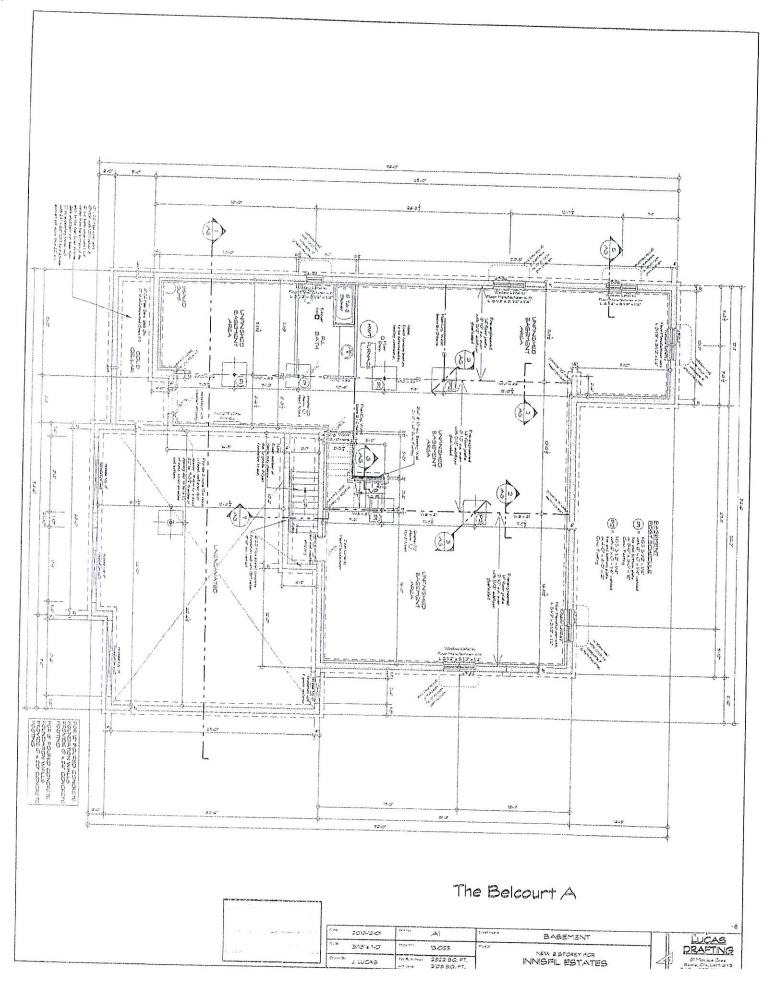
TOTAL 32

4 Bedrooms - 2000 L/D Fixture Count 32 = 600 L/D 272 m² = 800 L/D Q = 2800 T = 50





, eres



Schedule 3:	Sewage	System	Design	Specifications

1	ewage System	e Reside	Commercial							
Proposed Ty	pe of Sewade Svet	(C) (C)	Replac	ement	Repair/Alteration					
- ULASSZ	- Grainwater Queton									actori
E CLASS 4	- Leaching Rod Que	tem		CLASS	3-(Cesspo	201	and an a distant of the statements	*****	
Building Info	rmation	stern	0	CLASS	5-1	lolding) Ta	ank		
			an the second states of the second second							an a
Plumbing F	ixtures									
Description		Existing	+ Pr	oposed	Tel	Talal	7			
		J		opused	=	Total	X	Fixture	=	Count
Example; Sir	nk	0	+ 1			4		Units		
Bathroom Gr	oup		+	-	1=	1	X	1.5	=	1.5
Toilet/Sink/SI	hower			1	=	4	X	6	=	.700
Sinks/Wash I	Basins			1			$\left - \right $			24
Bathtub/Show	wers		+		=		X	1.5	=	1.5
Toilets (flush Dishwasher	tank)					/	X	1.5	-	1.5
Disriwasher			*	1		,	X	4.5	=	- 1000
Other:	Washing Machine		+	2	=	3		1.5	=	15
Ourier.			+		=	2	X	1.0		-3
				TO		EIVTI	X	EUNITS	=	
						MAN		UNITS	=	31.5
INSHEDEC		1-2-1		-						
		2/0/	m	2						
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esign Flow C BEDROOM F	Calculations (Q) LOWS					1077-11.002000000000	lattoente	THE CONTRACTOR OF THE	a na secondaria secondaria secondaria secondaria secondaria secondaria secondaria secondaria secondaria second	
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esign Flow C	Calculations (Q) LOWS # of Bedrooms 1 Bedroom 2 Bedrooms	Volume (Litres) 750 1100								
esign Flow C BEDROOM F	Calculations (Q)LOWS# of Bedrooms1 Bedroom2 Bedrooms3 Bedrooms	Volume (Litres) 750 1100 1600	Tota	I Flow) = A +	· (B	or C or E		₩
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A A A A A A DDITIONAL	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m ² over	Volume (Litres) 750 1100 1600 2000 2500		al Flow	A B C	+ A = ((B 90	or C or E		
A A A A DDITIONAL B	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m ² over 200m ² - 400m ²	Volume (Litres) 750 1100 1600 2000 2500 500		I Flow	A B C D	* A +	(B) 30 80 60	or C or E වෙත රාව රාව))	
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A A A A DDITIONAL B	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m² over 200m² - 400m² Each 10m² over 400m² - 600m²	Volume (Litres) 750 1100 2000 2500 500 100 75		al Flow	C A B C D E S) = A +		or C or E	DES	
A A A A DDITIONAL B	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m² over 200m² - 400m² Each 10m² over 400m² - 600m² Each 10m² over	Volume (Litres) 750 1100 1600 2000 2500 500		al Flow	C A B C D E S) = A +		or C or E	DES	
A A A A DDITIONAL B C	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m² over 200m² - 400m² Each 10m² over 400m² - 600m² Each 10m² over 600m² OR*	Volume (Litres) 750 1100 1600 2000 2500 500 100 75 50		al Flow	C A B C D E S) = A +		or C or E たら つと DAILY I	DES	
A A A A DDITIONAL B	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m² over 200m² - 400m² Each 10m² over 400m² - 600m² Each 10m² over 600m² OR* Each Fixture over	Volume (Litres) 750 1100 2000 2500 500 100 75	Tota Doc		C A B C D E S) = A +		or C or E	DES	
A A A A A A DDITIONAL B C D	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m² over 200m² - 400m² Each 10m² over 400m² - 600m² Each 10m² over 600m² OR* Each Fixture over 20 Fixture Units	Volume (Litres) 750 1100 1600 2000 2500 500 100 75 50 50		al Flow	C A B C D E S) = A +		or C or E	DES	
A A A A A A DDITIONAL B C D	Calculations (Q) LOWS # of Bedrooms 1 Bedrooms 2 Bedrooms 3 Bedrooms 4 Bedrooms 5 Bedrooms 5 Bedrooms FLOW FOR: Each Bedroom over 5 OR* Each 10m² over 200m² - 400m² Each 10m² over 400m² - 600m² Each 10m² over 600m² OR* Each Fixture over	Volume (Litres) 750 1100 1600 2000 2500 500 100 75 50 50			C A B C D E S) = A + = = = = XPEC EWAG _) & c		or C or E)) DES I = Per	

Schedule 3: Sewage System Design Specifications

A percolation septic system Percolation 1	Fest Comple	ted?	Yes	S					
*** Reguirem Perc	ents for "Per	rcolation Tes	t Dr.	and a accedur	analysis of ittached to p e" are attact	native ermit	e soil i applic	MUST be c ation)	ompleted
Τ :	of a contracted of the contrac	of Native S	OII		Per	colatio		te of Impori	
Test Pit A test pit shou and groundwa		and the second second second			posed leach a minimum d	ing be of 1m	d to c wide	bserve sub and 1.5m d	osoil profile eep.
Son Type	Coarse Gravel, No Fines	Gravel, Some Small Rocks	Gravel- Sand Mix, Some Fines		Sand, Fairly Uniform, Some Fines		andy- Silty- am Loam,		Clay Smears Well, Rolls into
Percolation Rate (T)	0 to 1	1 to 5	5 to		10 to 15	15 to	25	25 to 50	Ribbons >50
Soil Depth (meters)	Soil Type (See Above)	Percolatio Rate (T)	n	Rock	Depth of /Imperviou	s er	Dep	osoil to be	m
0.2					table		Usa Dep	able Existin	ng Soil: m
0.6 0.8 1.0		40					SOI		
1.2							Imp	th: <u>() (o</u> <u>t</u> e orted Fill: th: <u>() (S</u> te	
the second				*****			Dep	th: <u>6.3 k</u>	LOSM

? _____,

.

Schedule 3: Sewage System Design Specifications

ABSORPTION TRENCH	In-ground	@ Raised	Partially Raised					
Length of Distribution Pipe:								
$L = \underline{Q \times T}_{200}$		L =	m					
WATER Loo	a In-ground	Raised	Partially Raised					
lf Q ≤ 3000L	A=Q/75 Store	Effective Area = 38	<u> </u>					
lf Q > 3000L.	A = Q/50	Effective Area =	m²					
Extended Contact Area:								
$A = \underline{Q \times T}_{MOO}$	5-	Contact Area =	<u>350.</u> m²					
MANTLE/LOADING AREA								
Loading Rates (LR) Fill-Based Trenches and Filter Beds (Table 8.7.4.1. A OBC)								
Pe	ercolation Time of Soil (T) min/cm 1 < T ≤ 20	Loading Rates (L/m²/day)						
,	20 < T ≤ 35	<u> </u>						
V4	35 < T ≤ 50	6						
	T > 50	4						
Loading Area = Q/LR		Loading Area =	<u>67</u> m²					

or plumbing for an upper-tier municipality, board of health or conservation authority to whom this application is made, or, c) Director, Building and Development Branch, Ministry of Municipal Affairs and Housing 777 Bay St., 2nd Floor. Toronto, M5G 2E5 (416) 585-6666.

Schedule 1: Designer Information

Use one form for each individual who reviews and takes responsibility for design activities with respect to the project.

A. Project Information							
Building number, street name			Unit no.	Lot/con.			
Municipality		Plan number/ other desc	Anne and a second second second				
B. Individual who reviews and takes responsibility for design activities							
Name Jason Cheslock		Firm Rumball Excavation	5'				
Street address 408 Tiffin Street,	1		Unit no.	Lot/con.			
Municipality Barrie	L4N 5W8 Province ON		E-mail jscheslock@gmail.com				
Telephone number (705)722-1145	Fax number (705)735-1701		Cell number (705) 623-3889				
C. Design activities undertaken l	by individua	I identified in Section					
3.5.2.1. of Division C]							
House Small Buildings		– House ng Services	 Building S Plumbing 				
 Small Buildings Large Buildings 	Detect	tion, Lighting and	Plumbing – All Buildings				
Complex Buildings	Power			ewage System			
Description of designer's work	G Fire P	rotection					
D. Declaration of Designer IJason Cheslockdeclare that (choose one as appropriate): (print name) I review and take responsibility for the design work on behalf of a firm registered under subsection 3.2.4. of Division C, of the Building Code. I am qualified, and the firm is registered, in the appropriate classes/categories. Individual BCIN: 10457							
I review and take responsibility for the design and am qualified in the appropriate category as an "other designer" under subsection 3.2.5.of Division C, of the Building Code. Individual BCIN: Basis for exemption from registration:							
The design work is exempt from the registration and qualification requirements of the Building Code. Basis for exemption from registration and qualification: I certify that:							
	nis schedule is	true to the best of my kno	owledae.				
 The information contained in this schedule is true to the best of my knowledge. I have submitted this application with the knowledge and consent of the firm. 							
Nov 27 2018 Date	(fles	Signature of Design	er			
NOTE:	/						

1. For the purposes of this form, "individual" means the person" referred to in Clause 3.2.4.7(1) d) of Division C, Article 3.2.5.1. of Division C, and all other persons who are exempt from qualification under Subsections 3.2.4. and 3.2.5. of Division C. Application for a Permit to Construct or Demolish – Effective January 1, 2011

2. Schedule 1 is not required to be completed by a holder of a license, temporary license, or a certificate of practice, issued by the Ontario Association of Architects. Schedule 1 is also not required to be completed by a holder of a license to practise, a limited license to practise, or a certificate of authorization, issued by the Association of Professional Engineers of Ontario.

Schedule 2: Sewage System Installer Information

A. Project Information					
Building number, street name			Unit number	Lot/con.	
Municipality	Postal code	Plan number/ other description			
Sewage system installer					
Is the installer of the sewage sys cleaning or emptying sewage sys Ves (Continue to Section	stems, in accordar n C) No (Contine	nce with Building Co ue to Section E)	de Article 3.3.1.1, Div Installer unkno (Continue to Se	rision C? wn at time of applicatior	
Registered installer informa		swer to B is "Yes	7		
Name Rumball Excavation and H	laulage		BCIN 10457		
Street address 408 Tiffin Street		Unit number	Lot/con.		
Municipality Barrie	Postal code L4N 5W8	Province ON		ock@gmail.com	
Telephone number (705)722-1145	Fax (705)735-	1701	Cell number (705) 62	3-3889	
Qualified supervisor inform					
Name of qualified supervisor(s)	IN)				
		10457			
J Cheslock		10456			
R Cheslock			والمستحين والمرواحية بعروم فرحيه والمروح والمتعاولة والمعاولة والمعارية والمروح والمروح والمروح والمروح والمروح		
Declaration of Applicant:					
Jason Cheslock			declare that:		
	name)		ue	ciare triat.	
I am the applicant for application, I shall sub	the permit to cons omit a new Schedu	truct the sewage sys lle 2 prior to construc	tem. If the installer is to the installer is to the installe	s unknown at time of er is known;	
I am the holder of the that the installer is known	permit to construc own.	t the sewage system	n, and am submitting	a new Schedule 2, now	
I certify that:					
1. The information contain	ed in this schedul	e is true to the best o	of my knowledge.		
2. If the owner is a corpora	ation or partnershi	p, I have the authorit	y to bind the corpora	tion or partnership.	
Nov 27 2018 Date	/	Al	Signature of ap	oplicant	

Lot 28 Building Permit No.: 2018-0850

BUILDING PERMIT

Number: 2018-0850

Schedule a Building Inspection:

Please book your inspection(s) online by clicking this link: <u>www.innisfil.ca/eservices</u> or Email: buildinginspections@innisfil.ca or Leave a phone message at: 705-436-3710 Ext. 3500

Applicant : Owner : Legal Description : Roll Number :

Sigmund Tronowicz, Ant Construction 1820839 ONTARIO INC PLAN 51M1045 LOT 28 010035054380000

Inspections Required:

- Sewage System Readiness to Construct
- Sewage System Substantial Completion
- Notice of Completion

Conditions/Remarks:

New Septic Installation Water-Loo Wire Mesh Model 20

Maintenance agreement required for treatment system

Alarm Test required

Provide granular analysis for native and imported soil prior to install inspection.

Ensure header and distribution piping is able to be detected magnetically via 14 gauge tracer wire or other means.

Ensure distribution piping and septic tank are minimum distance from all wells and property lines.

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